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Aerodynamic Influence Coefficients from Supersonic Strip Theory: Analytical Development and Computational Procedure

1 AUGUST 1962

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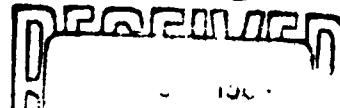
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Prepared for COMMANDER SPACE SYSTEMS DIVISION

UNITED STATES AIR FORCE

Inglewood, California

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(6) AERODYNAMIC INFLUENCE COEFFICIENTS FROM
SUPersonic STRIP THEORY: ANALYTICAL DEVELOPMENT
AND COMPUTATIONAL PROCEDURE

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VII

AERODYNAMIC INFLUENCE COEFFICIENTS FROM
SUPERSONIC STRIP THEORY: ANALYTICAL DEVELOPMENT
AND COMPUTATIONAL PROCEDURE

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ABSTRACT

In this report, we review a method for computing the aerodynamic influence coefficients (AICs) for surfaces with supersonic leading edges. The method is based on the two-dimensional second-order potential solution of Van Dyke. The strip oscillatory coefficients are obtained from the extension of Van Dyke's work by Rodden and Revell to include the effects of sweep and finite span in addition to the effects of thickness, leading to a method that will avoid the unconservatism of linearized theory and will be applicable at Mach numbers below the lower Mach number limit of piston theory.

The influence coefficients relate the aerodynamic forces to the surface deflections through the following definitions. In the oscillatory case,

$$\{F\} = \rho \omega^2 b_r^2 s [C_h] \{h\}$$

and in the steady case,

$$\{F_s\} = (1/2) \rho V^2 (S/c) [C_{hs}] \{h\}$$

The Aerospace IBM 7090 Computer Program No. HM10 provides the AICs in printed and optional punched-card output formats. The theoretical formulation is limited to Mach numbers normal to the leading edge greater than 1.25. The program capacity is 25 surface strips, 25 values of Mach number, and 50 values of reduced velocity.

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SYMBOLS

A_n, B_n, C_n, D_n	Coefficients in series expansion for oscillatory aerodynamic coefficients
a_{ij}	Coefficients in series expansion of pressure coefficients
b	Local semichord
b_r	Reference semichord
C_h	Element of oscillatory aerodynamic influence coefficient matrix
C_{hs}	Element of steady aerodynamic influence coefficient matrix
c	Local chord
\bar{c}	Mean aerodynamic chord
c_r	Root chord
c_t	Tip chord
d	Distance between forward and aft control points
F	Control point force
f_n	Finite span correction factors
g	Airfoil semithickness
h	Vertical deflection
I_n, J_n, K_n, L_n	Thickness integrals
k	Local reduced frequency, $k = \omega b/V$
k_r	Reference reduced frequency
L_{h_o}, L_{a_o}	Oscillatory leading edge lift coefficients
L_o	Lift referred to leading edge motion
M	Freestream Mach number

\bar{M}	Normal Mach number, $\bar{M} = M \cos \Lambda$
M_{h_o}, M_{a_o}	Oscillatory leading edge moment coefficients
M_o	Moment about leading edge
N	$= [(\gamma+1)/2] (M/\beta)^2$
\bar{N}	$= [(\gamma+1)/2] (\bar{M}/\bar{\beta})^2$
r	$= \tau_{te}/\tau$
S	Wing area
s	Wing semispan
V	Free stream velocity
$V/b_r \omega$	Reference reduced velocity, $V/b_r \omega = 1/k_r$
x, ξ	Streamwise coordinates
x_m	Chordwise location of point of maximum thickness
α	Angle of attack
β	$= (M^2 - 1)^{1/2}$
$\bar{\beta}$	$= (\bar{M}^2 - 1)^{1/2}$
γ	Specific heat ratio of air ($\gamma = 1.400$)
Δy	Strip width
Λ	Leading edge sweep angle
λ	Trailing edge sweep angle
ρ	Free stream density
τ	Airfoil maximum thickness ratio
τ_{te}	Airfoil trailing edge thickness ratio
ω	Circular frequency
[]	Square matrix
{ }	Column matrix

SECTION I

FORMULATION OF PROBLEM

A. Introduction

For aeroelastic analyses of surfaces with supersonic leading edges, a strip theory is desirable that will avoid the unconservatism of linearized theory and will be applicable at lower Mach numbers than piston theory. The second-order theory of Van Dyke¹ offers such a possibility, and it can be shown² that both the linearized theory and the piston theory are special cases of this solution.

Van Dyke's analysis is the result of both an iteration and a frequency expansion in the solution of the nonlinear, unsteady potential equation. The iteration has been carried through to obtain the second-order velocity potential (first-order in thickness), and the frequency expansion has been extended to the cubic term. The result has been presented in a series form for the local pressure coefficient on the airfoil; no control surface has been considered.

The present formulation makes use of the pressure coefficient as integrated by Rodden and Revell,² corrected for sweep and finite span. The AICs for strip theory have been discussed in Ref. 3 considering quarter-chord coefficients; a more convenient derivation utilizing leading edge coefficients is given in the present study. The computational aspects of this report are an extension of work previously discussed in Ref. 4.

B. Sign Convention

The flutter sign convention is used in the oscillatory case: forces and deflections are positive down; rotations are positive with leading edge up. The aerodynamic sign convention is used in the steady case: forces and deflections are positive up, rotations are positive with leading edge up.

C. Derivation of Equations

The derivation is based on the defining equation for the matrix of oscillatory AICs

$$\{F\} = \rho \omega^2 b_r^2 s [C_h] \{h\}$$

The steady AICs are defined by

$$\{F_s\} = (1/2) \rho V^2 (S/\bar{c}) [C_{hs}] \{h\}$$

and will be obtained from the limit of the oscillatory case

$$[C_{hs}] = \lim_{k_r \rightarrow 0} 2k_r^2 (\bar{sc}/S) [C_h]$$

We shall derive the aerodynamic matrix for only a single strip since strip theory leads to a partitioned form for the entire surface; e.g.,

$$[C_h] = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & C_{h1} & 0 & 0 \\ 0 & 0 & C_{h2} & 0 \\ 0 & 0 & 0 & C_{h3} \end{bmatrix}$$

in the case of a three-strip wing where the first null partition is reserved for control points whose aerodynamic forces can be neglected (e.g., external stores). Each surface partition is of the order 2×2 since we consider only

the degrees of freedom in pitching and plunging: the Van Dyke solution has not yet been extended to the control surface degree of freedom. The given and equivalent force systems and geometry are shown in Fig. 1. The forward control point in the equivalent system has been arbitrarily placed in the quarter chord location.

The force equivalence is given by

$$\begin{bmatrix} 1 & 1 \\ b/2 & (d+b/2) \end{bmatrix} \begin{Bmatrix} F_1 \\ F_2 \end{Bmatrix} = \begin{Bmatrix} L_o \\ M_o \end{Bmatrix}$$

from which

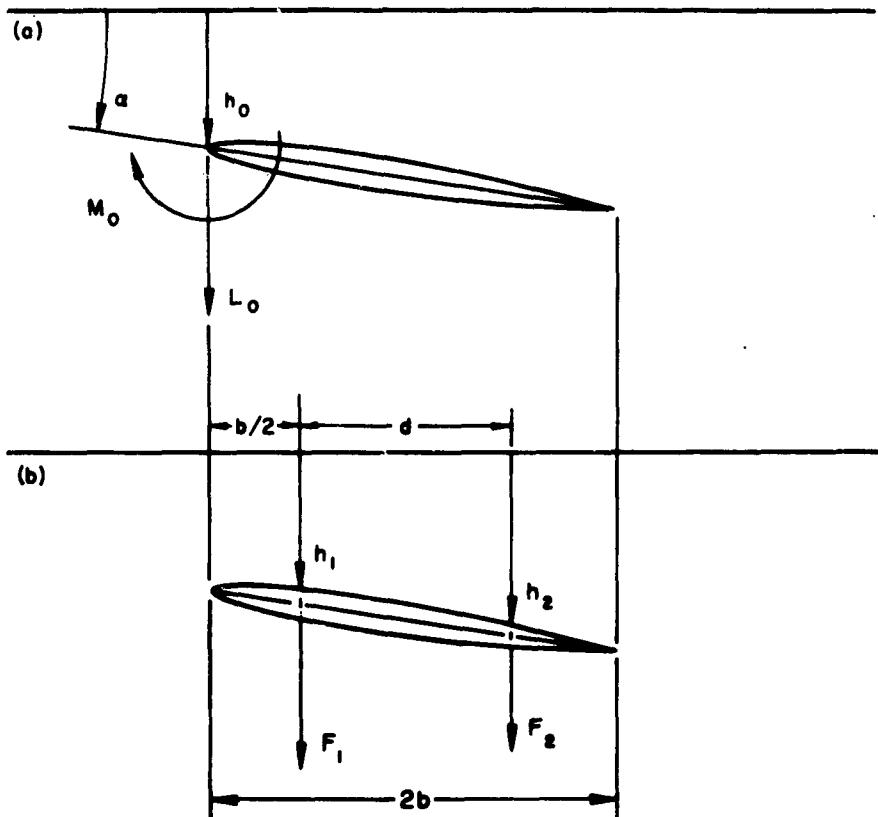
$$\begin{Bmatrix} F_1 \\ F_2 \end{Bmatrix} = \begin{bmatrix} (1+b/2d) & -1/d \\ -b/2d & 1/d \end{bmatrix} \begin{Bmatrix} L_o \\ M_o \end{Bmatrix}$$

The leading edge oscillatory coefficients are defined by

$$\begin{Bmatrix} L_o \\ M_o \end{Bmatrix} = 4\rho\omega^2 b^2 \Delta y \begin{bmatrix} 1 & 0 \\ 0 & b \end{bmatrix} \begin{bmatrix} L_{h_o} & L_{a_o} \\ M_{h_o} & M_{a_o} \end{bmatrix} \begin{Bmatrix} h_o \\ b.a \end{Bmatrix}$$

The geometrical equivalence is

$$\begin{Bmatrix} h_o \\ b.a \end{Bmatrix} = \begin{bmatrix} (1+b/2d) & -b/2d \\ -b/d & b/d \end{bmatrix} \begin{Bmatrix} h_1 \\ h_2 \end{Bmatrix}$$



**Fig. 1. Original (a) and Equivalent (b)
Force Systems and Geometry.**

Cascading the above solutions we find

$$\begin{Bmatrix} F_1 \\ F_2 \end{Bmatrix} = 4\rho\omega^2 b^2 \Delta y \begin{bmatrix} (1+b/2d) & -b/d \\ -b/2d & b/d \end{bmatrix}$$

$$x \begin{bmatrix} L_{h_o} & L_{a_o} \\ M_{h_o} & M_{a_o} \end{bmatrix} \begin{bmatrix} (1+b/2d) & -b/2d \\ -b/d & b/d \end{bmatrix} \begin{Bmatrix} h_1 \\ h_2 \end{Bmatrix}$$

Comparing this result to the definition of the influence coefficient matrix, we find

$$[C_h] = 4(b/b_r)^2 (\Delta y/s) \begin{bmatrix} (1+b/2d) & -b/d \\ -b/2d & b/d \end{bmatrix}$$

$$x \begin{bmatrix} L_{h_o} & L_{a_o} \\ M_{h_o} & M_{a_o} \end{bmatrix} \begin{bmatrix} (1+b/2d) & -b/2d \\ -b/d & b/d \end{bmatrix}$$

We note the pre- and post-multipliers to be mutual transposes. Once the partitions have been obtained for each strip, the total matrix is formed as indicated above.

The steady influence coefficients follow as a limiting case of the oscillatory matrix. From the definitions of both oscillatory and steady matrices we find (since in both sign conventions the forces and deflections are in the same direction)

$$[C_{hs}] = \lim_{k_r \rightarrow 0} 2k_r^2 (s\bar{c}/s) [C_h]$$

We next consider the oscillatory coefficients necessary in the influence coefficient formulation. Space permits only a summary of the results given by Ref. 2. The strip leading edge oscillatory coefficients are given by

$$L_{h_0} = A_2 f_2 + i(A_3 f_1/k + A_4 f_3 k)$$

$$L_{a_0} = (B_1 f_1/k^2 + B_2 f_3) + i(B_3 f_2/k + B_4 f_4 k)$$

$$M_{h_0} = C_2 f_3 + i(C_3 f_2/k + C_4 f_4 k)$$

$$M_{a_0} = (D_1 f_2/k^2 + D_2 f_4) + i(D_3 f_3/k + D_4 f_5 k)$$

where A_n , B_n , C_n , and D_n depend on the Mach number and airfoil thickness integrals, the f_n are finite span correction factors, and the reduced frequency k is based on the local chord.

The basic expressions involved in A_n , B_n , C_n , and D_n can be outlined, but the reader is referred to Ref. 2 for the finite span correction factors f_n (it may be noted that the $f_n = 1$ for all strips inboard of the tip Mach cone, whereas as the $f_n < 1$ in the region of the tip Mach cone). The basic expressions are

$$A_2 = -(1/8)(a_{22}/2 + J_1 a_{24} + I_2 a_{26})$$

$$A_3 = -(1/8)(a_{12} + I_1 a_{14})$$

$$A_4 = -(1/8)(a_{32}/3 + K_1 a_{34} + J_2 a_{36} + I_3 a_{38})$$

$$B_1 = (1/4)(a_{01} + I_1 a_{02})$$

$$B_2 = (1/4)(a_{21}/3 + K_1 a_{23} + J_2 a_{25} + I_3 a_{27})$$

$$B_3 = (1/4)(a_{11}/2 + J_1 a_{13} + I_2 a_{15})$$

$$B_4 = (1/4)(a_{31}/4 + L_1 a_{33} + K_2 a_{35} + J_3 a_{37} + I_4 a_{39})$$

$$C_2 = -(1/4) (a_{22}/3 + J_2 a_{24} + I_3 a_{26})$$

$$C_3 = -(1/4) (a_{12}/2 + I_2 a_{14})$$

$$C_4 = -(1/4) (a_{32}/4 + K_2 a_{34} + J_3 a_{36} + I_4 a_{38})$$

$$D_1 = (1/2) (a_{01}/2 + I_2 a_{02})$$

$$D_2 = (1/2) (a_{21}/4 + K_2 a_{23} + J_3 a_{25} + I_4 a_{27})$$

$$D_3 = (1/2) (a_{11}/3 + J_2 a_{13} + I_3 a_{15})$$

$$D_4 = (1/2) (a_{31}/5 + L_2 a_{33} + K_3 a_{35} + J_4 a_{37} + I_5 a_{39})$$

where

$$a_{01} = - (4/\bar{\beta}) \cos \Lambda$$

$$a_{02} = - (4/\bar{\beta}^2) (\bar{M}^2 \bar{N} - 2)$$

$$a_{11} = (8/\bar{\beta}^3) (2 - \bar{M}^2) \cos \Lambda$$

$$a_{12} = (8/\bar{\beta}) \cos \Lambda$$

$$a_{13} = (16\bar{M}^2/\bar{\beta}^4) (\bar{N} - 1)$$

$$a_{14} = (8/\bar{\beta}^2) (\bar{M}^2 \bar{N} - 2)$$

$$a_{15} = (8/\bar{\beta}^4) (2 - \bar{M}^2) (\bar{M}^2 \bar{N} - 1)$$

$$a_{21} = (4/\bar{\beta}^5) (\bar{M}^2 + 2) \cos \Lambda$$

$$a_{22} = (16/\bar{\beta}^3) \cos \Lambda$$

$$a_{23} = (8\bar{M}^2/\bar{\beta}^6) [3(3\bar{M}^2 - 2) \bar{N} - 2(5\bar{M}^2 - 3)]$$

$$a_{24} = (8\bar{M}^2/\bar{\beta}^4) (4\bar{N} - 5)$$

$$a_{25} = (4\bar{M}^2/\bar{\beta}^6) [(16 - 7\bar{M}^2)\bar{N} + 4(2\bar{M}^2 - 3)]$$

$$a_{26} = (16\bar{M}^2/\bar{\beta}^4) (\bar{N} - 1)$$

$$a_{27} = (4\bar{M}^2/\bar{\beta}^6) [(\bar{M}^2 + 2)\bar{N} - 4]$$

$$a_{31} = -(8\bar{M}^2/3\bar{\beta}^7) (\bar{M}^2 + 4) \cos \Lambda$$

$$a_{32} = -(24\bar{M}^2/\bar{\beta}^5) \cos \Lambda$$

$$a_{33} = (16\bar{M}^2/\bar{\beta}^8) [(17\bar{M}^4 - 10\bar{M}^2 - 4)\bar{N} - (5\bar{M}^2 - 2)(4\bar{M}^2 - 1)]$$

$$a_{34} = (16\bar{M}^2/\bar{\beta}^6) [6\bar{M}^2 - (5\bar{M}^2 - 2)\bar{N}]$$

$$a_{35} = (16\bar{M}^2/\bar{\beta}^8) [7\bar{M}^2(2\bar{M}^2 - 1) - (12\bar{M}^4 - 3\bar{M}^2 - 4)\bar{N}]$$

$$a_{36} = (8\bar{M}^2/\bar{\beta}^6) [2(\bar{M}^2 + 1) - (\bar{M}^2 + 8)\bar{N}]$$

$$a_{37} = (8\bar{M}^2/\bar{\beta}^8) [(3\bar{M}^2 + 2) - (3\bar{M}^2 + 4)\bar{N}]$$

$$a_{38} = (8\bar{M}^2/\bar{\beta}^6) [2(\bar{M}^2 + 1) - 3\bar{M}^2\bar{N}]$$

$$a_{39} = (8\bar{M}^2/3\bar{\beta}^8) [(5\bar{M}^2 + 2) - \bar{M}^2\bar{N}(\bar{M}^2 + 4)]$$

and the thickness integrals are defined by

$$I_n = (1/2b)^n \int_0^{2b} x^{n-1} g' dx, \quad n = 1(1)5$$

$$J_n = (1/2b)^{n+1} \int_0^{2b} x^{n-1} g dx, \quad n = 1(1)4$$

$$K_n = (1/2b)^{n+2} \int_0^{2b} x^{n-1} dx \int_0^x g d\xi, \quad n = 1(1)3$$

$$L_n = (1/2b)^{n+3} \int_0^{2b} x^{n-1} dx \int_0^x \xi g d\xi, \quad n = 1(1)2$$

Reference 2 evaluates these thickness integrals for a typical airfoil.

From the oscillatory coefficient expressions we may find the limiting values and the steady matrix for a single strip

$$\begin{aligned} [C_{hs}] &= 8(\bar{s}/S) (\Delta y/s) \begin{bmatrix} (1+b/2d) & -b/d \\ -b/2d & b/d \end{bmatrix} \\ &\times \begin{bmatrix} 0 & B_1 f_1 \\ 0 & D_1 f_2 \end{bmatrix} \begin{bmatrix} (1+b/2d) & -b/2d \\ -b/d & b/d \end{bmatrix} \end{aligned}$$

D. References

1. M. D. Van Dyke. "Supersonic Flow Past Oscillating Airfoils Including Nonlinear Thickness Effects." NACA TN 2982, 1953.
2. W. P. Rodden and J. D. Revell. "Oscillatory Aerodynamic Coefficients for a Unified Supersonic Hypersonic Strip Theory." Journal of the Aerospace Sciences, 27 (1960), 451; based on North American Aviation, Inc., Report NA-57-1549, 31 December 1957.

3. W. P. Rodden. "Aerodynamic Influence Coefficients from Strip Theory." Journal of the Aerospace Sciences, 26 (1959), 833.
4. W. P. Rodden, E. F. Farkas, and R. K. Oyama. "Aerodynamic Influence Coefficients by Supersonic Strip Theory: Analytical Development and Procedure for the IBM 7090 Computer." Norair Division, Northrop Corporation, Report NOR-61-56, 14 April 1961.

SECTION II
GENERAL DESCRIPTION OF INPUT

A. Units

Since all dimensional input is geometrical and the aerodynamic matrix is dimensionless, only a consistent set of length units is necessary: inches or feet.

B. Classes of Numerical Data and Limitations

The data required by the program are the geometry, reduced velocities, and Mach numbers. The example illustrates their use.

1. Example Problem

We consider the four-strip wing shown in Fig. 2 at the freestream Mach numbers of 1.8 and 2.5 for the reduced velocities of 4.0 and 8.0 and the steady case. The aerodynamic matrices will be found with and without the tip correction, and the thickness integrals will be generated by the program from the expressions of App. A of Ref. 2 for an assumed airfoil (constant across the span) having 10 percent thickness, maximum thickness at 40 percent chord, and a blunt trailing edge that has a trailing-edge-to-maximum-thickness ratio of 0.15.

2. Program Restrictions and Options

a. The number of strips into which a wing may be subdivided must be < 25.

b. The number of reduced velocities used for any one Mach number must be < 50.

c. The number of values of Mach number must be < 25.

d. If it is desired to compute the steady matrix [C_{hs}], a zero or negative value of $V/b_r \omega$ must be used and S and \bar{c} must also be supplied.

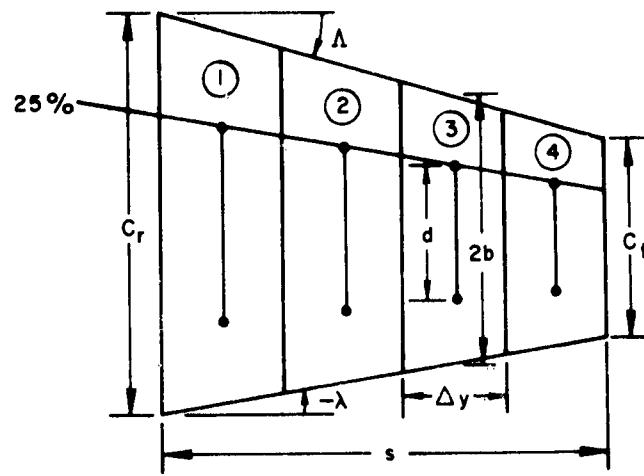


Fig. 2. Example of Four-Strip Wing.

<u>Strip No.</u>	<u>Δy (ft)</u>	<u>b (ft)</u>	<u>d (ft)</u>
1	4.7	12.28125	11.9
2	4.2	9.50000	9.0
3	3.6	7.06250	6.6
4	3.1	4.96875	4.5

$$b_r = 6.5 \text{ ft}$$

$$s = 15.6 \text{ ft}$$

$$c_r = 27.5 \text{ ft}$$

$$c_t = 8.0 \text{ ft}$$

$$\tan \Lambda = 0.75 (\cos \Lambda = 0.80)$$

$$\tan \lambda = -0.50$$

$$\bar{c} = 21.0 \text{ ft}$$

$$S = 554.0 \text{ sq ft}$$

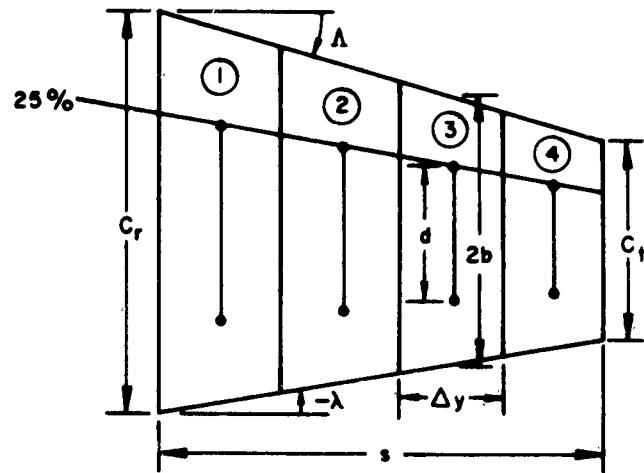


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2	4.2	9.50000	9.0
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4	3.1	4.96875	4.5

$$b_r = 6.5 \text{ ft}$$

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$$\tan \Lambda = 0.75 (\cos \Lambda = 0.80)$$

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$$\bar{c} = 21.0 \text{ ft}$$

$$S = 554.0 \text{ sq ft}$$

SECTION III

DATA DECK SETUP

A. Loading Order

Input decks punched from keypunch forms are loaded behind column binary deck HM10. Any number of complete decks may be stacked. The data for each deck must be in the following order:

- (1) Heading Card 1
- (2) Heading Card 2
- (3) ISTRIP, JMACH, KVBRW, ISTHK, ISTIP, NO PUNJ
- (4) b_r , s , S , \bar{c} , c_t , $\tan \Lambda$, $\tan \lambda$, $\cos \Lambda$
- (5) b_i series
- (6) d_i series
- (7) Δy_i series
- (8) M_j series
- (9) $(V/b_r \omega)_k$ series
- (10) Thickness integrals
 - (a) Provide thickness integrals
 - (b) Input data to compute thickness integrals

B. Input Data Description

- (1) Heading Card 1 may contain any information desired (Columns 2 through 72). Column 1 should be blank.
- (2) Heading Card 2 provides for more information (Columns 2 through 72): vehicle, date, name. Column 1 is blank and all or any of the fields may be blank but the card must be included.

- (3) Control card (FORMAT 1814)
- (a) ISTRIP = number of strips
 - (b) JMACH = number of Mach numbers
 - (c) KVBRW = number of reduced velocities
 - (d) ISTHK = 0 if thickness integrals are tabulated
= 1 if x_m/c , τ , and r are constant
= 2 if x_m/c and r are constant and τ
varies with each strip
= 3 if x_m/c , τ , and r all vary with each strip
 - (e) ISTIP = 0 if tip correction factor is 1.0
≠ 0 if tip correction factor is to be computed
by program
 - (f) NO PUNJ = 0 or blank if the computed matrices are
to be punched in cards
≠ 0 if no punched cards are desired
- (4) Single parameters (FORMAT 6E12.8): When computing both steady-state and oscillatory AICs from the same data deck, we use the eight parameters: b_r (semichord), s (semispan), S (surface area), \bar{c} (mean aerodynamic chord), c_t (tip chord), $\tan \Lambda$ (tangent of leading edge sweep angle), $\tan \lambda$ (tangent of trailing edge sweep angle), and $\cos \Lambda$ (cosine of leading edge sweep angle). For computing oscillatory cases, S and \bar{c} may be blank (or included); and for steady cases, b_r and s may be blank (or included). These parameters are tabulated in the same order as defined, and always require two lines (cards).
- (5), (6), and (7) Series b_i , d_i , and Δy_i (FORMAT 6E12.8): The number of lines (cards) required by the b_i , d_i , and Δy_i series is controlled by the number of strips. Using the maximum 25 strips would require five cards for each series. Tabulate b_i (local semichords), d_i (distance between control points), and

Δy_i (strip widths) in the order defined with each new series starting on a new card.

- (8) and (9) M_j (freestream Mach number) and $V/b_r \omega$ (reduced velocity) series (FORMAT 6E12.8): The M_j series may be input in any order desired with $j \leq 25$ per deck. $M_j \cos \Lambda$ must be ≥ 1.25 . The $(V/b_r \omega)_k$ series is tabulated only once per deck and will be repeated by the program for each Mach number indicated by the M_j series. For the steady case, tabulate either a zero or negative $V/b_r \omega$.
- (10) Thickness integral input (FORMAT 6E12.8)
- (a) $ISTHK = 0$; the thickness integrals must be tabulated in the order: $I_1, I_2, I_3, I_4, I_5, J_1, J_2, J_3, J_4, K_1, K_2, K_3, L_1$, and L_2 (three cards).
- (b) $ISTHK \neq 0$; the thickness integrals are computed by supplying x_m/c (percent chord location of maximum thickness; τ (airfoil maximum thickness ratio), and r (ratio of τ_{te}/τ). When using this option omit (10.a):
- 1) $ISTHK = 1$; the three ratios are each constant for the surface and tabulated in the order defined. (First field in three separate cards.)
 - 2) $ISTHK = 2$; the ratios x_m/c and r are each constant for the surface but τ varies with each strip. Input in the order x_m/c , (Field 1, first thickness integral card), τ series (beginning on a new card), and r (Field 1 of the last card).

3) ISTHK = 3; the ratios x_m/c , τ , and r all vary with each strip. Tabulate in order with each new series starting on a new card.

C. Example Keypunch Forms

Example keypunch forms are given on the following pages. Columns 73 through 80 are reserved for data deck identification. This space may be used in any fashion; however, it is suggested that the last three columns be used for sequencing. Only the cards with sequencing in Columns 73 through 80 are to be used in the sample data deck; the lines (cards) with Columns 73 through 80 blank are for clarification of input.

80 COLUMN FREE KEYPUNCH



AEROSPACE CORPORATION

KEYPUNCHED
PROGRAMMER

MEET

DATE

VERIFIED

卷之三

PR

SAMPLE CASE WITHOUT TIP CORRECTION
W. P. RUGODEN APR. 1962

Heading
C O N S O L I D A T E D

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28

三

27

三

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47

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17

8 COLUMN FREE KEYPUNCH

PERFORATED

KEYPUNCHED

DATE

SHEET

NUMBER

AEROSPACE CORPORATION



EIGHT COLUMNS OF DATA FOR POINTS BETWEEN CONTROL POINTS (d)	
d_1	+0.1 +0.5
d_7	+0.1 +0.5
d_{13}	+0.1 +0.5
d_{19}	+0.1 +0.5
d_{25}	+0.1 +0.5
SIXTEEN COLUMNS OF DATA FOR MACH NUMBERS (M)	
ΔY_1	+0.7
ΔY_7	+0.1 +4.2
ΔY_{13}	+0.1 +3.1 +3.6
ΔY_{19}	+0.1 +3.1 +3.6
ΔY_{25}	+0.1 +3.1 +3.6
MACH NUMBERS (M)	
M_1	+1.0
M_7	+0.1 +2.5
M_{13}	+0.1 +2.5
M_{19}	+0.1 +2.5
M_{25}	+0.1 +2.5



80 COLUMN FREE KEYPUNCH

AEROSPACE CORPORATION

SHEET _____

DATE

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FRENCHED

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H M I 000 000 000

REDUCED VELOCITY (V/b_{∞}) = $(1/k_1) x$

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
---	---	---	---	---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	-----

$$0 + 0 = 0$$

1

13

1

25

31

37

3

8

THE JOURNAL OF CLIMATE

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K.

42

1

1

1

1

1

80 COLUMN FREE KEYPUNCH

PROGRAMMER _____

KEYPUNCHED _____

VERIFIED _____

DATE _____ SHEET _____



THICKNESS INTEGRAL CONTROL #0 ENTER THE PROPER NUMBER OF (x _n /c), r ₁ AND r ₂							
HMI 00001							
$(\frac{x_n}{c})$	+00	+00	+00	r ₁	r ₁	r ₁	HMI 000012
7				7	7	7	
13				13	13	13	
19				19	19	19	
25	+1	+00	+00	25	25	25	HMI 000013
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19	19	
				25	25	25	
				r ₁	r ₁	r ₁	
				7	7	7	
				13	13	13	
				19	19		

COLUMN FREE PUNCH

AEROSPACE CORPORATION

SAMPLE CLASS		WITH TIP CORRECTION		HMGACO	
N	F	R DODEN			
4	5				
+6.5	+ 0.1 + 15.6	+ 0.2 + 5.54	+ 3 + 2.1	+ 0.28	+ 0.0 + 7.5
-5	+ 9.6 + 6.8	+ 0.0			
0	- 2 + 9 + 2.5	+ 0.2 + 9.7	+ 3 + 7.0625	+ 0.1 + 4.96875	+ 0.1
1	+ 7	+ 0.2 + 9	+ 0.1 + 6.6	+ 0.1 + 4.5	+ 0.1
2	+ 4.7	+ 0.1 + 4.2	+ 0.1 + 3.6	+ 0.1 + 3.1	+ 0.1
3	+ 8	+ 0.1 + 7.8	+ 0.1	+ 0.1	+ 0.1
4	+ 6	+ 0.1 + 6.8	+ 0.1	+ 0.1	+ 0.1
5	+ 4	+ 0.1 + 5.4	+ 0.1	+ 0.1	+ 0.1
6	+ 4	+ 0.1 + 4.8	+ 0.1	+ 0.1	+ 0.1
7	+ 4	+ 0.1 + 4.2	+ 0.1	+ 0.1	+ 0.1
8	+ 4	+ 0.1 + 3.6	+ 0.1	+ 0.1	+ 0.1
9	+ 4	+ 0.1 + 3.1	+ 0.1	+ 0.1	+ 0.1
10	+ 4	+ 0.1 + 2.5	+ 0.1	+ 0.1	+ 0.1
11	+ 4	+ 0.1 + 1.9	+ 0.1	+ 0.1	+ 0.1
12	+ 4	+ 0.1 + 1.3	+ 0.1	+ 0.1	+ 0.1
					HMGACO
					13

SECTION IV
PROGRAM OUTPUT

A. Printed Output

1. All input data.
2. Each group of AICs with the associated Mach number and $V/b_r \omega$.
3. Sequencing number of the first and last punched cards (output) for each group (one $V/b_r \omega$) of influence coefficients.
4. Example problem printed output is given on the following pages.

AERODYNAMIC INFLUENCE COEFFICIENTS BY SUPERSONIC STRIP THEORY

INPUT DATA

* STRESSES
? BACH NUMBERS
INCLINED FREQUENCIES

COSINE LAMBDA =	0.80000000E 00
B(R) =	0.64999999E 01
S =	0.15625000E 02
G =	0.35460600E 03
COS R =	0.26999999E 02
C(T) =	0.80000000E 01
TAN LD =	0.75000000E 00
TAN TR =	-0.50000000E 00

SECTION TWO-CORRECTION

DELTA Y (I)	B(I)	D(I)
0.46999999E 01	0.12281249E 02	0.11900000E 02
0.31622776E 01	0.95000000E 01	0.90000000E 01
0.23572689E 01	0.74625000E 01	0.69599999E 01
0.16999999E 01	0.54687500E 01	0.49500000E 01
1/K (R) =	0.80000000E 01	0.
R =	0.40000000E 00	
MU =	0.10999999E 00	

SECTION THREE

CONSTANTS	I1(K)	I2(K)	I3(K)	I4(K)	I5(K)	J1(K)	J2(K)	J3(K)	J4(K)	K1(K)	K2(K)	K3(K)	L1(K)	L2(K)
0.74999999E-02	-0.27333333E-01	-0.26716665E-01	-0.23411199E-01	-0.20409866E-01	0.34833332E-01	0.17108332E-01								
J3(K)	J4(K)													
0.000000E+00	0.000000E+00	0.12264666E-01	0.17124999E-01	0.22052086E-01	0.68043330E-02	0.50654332E-02								

AERODYNAMIC INFLUENCE COEFFICIENTS BY SUPERSONIC STRIP THEORY

OSCILLATORY CASE

$$1/K(R) = 0.40000000E 01$$

$$0.11999999E 01$$

$$NUMBER OF STREAMS = 4$$

CH(1) SIZE = 2 BY 2	
0.82001874E 01 -0.85972560E 011	-0.94911763E 01 0.-40570676E 011
-0.58696458E 01 0.73110541E 011	0.34727361E 01 -0.60698704E 011

CH(2) SIZE = 2 BY 2	
0.14538863E 01 -0.18207212E 011	0.14304339E-00 -0.19185340E 011

CH(3) SIZE = 2 BY 2	
0.72746900E 01 -0.24152532E 011	0.1276747E 011
0.23201058E 01 -0.78480651E 001	-0.11905624E-001

CH(4) SIZE = 2 BY 2	
0.72746900E 01 -0.24152532E 011	-0.73959825E 01 0.11276747E 011
0.23201058E 01 -0.78480651E 001	-0.25969680E 01 0.31905624E-001

NUMBER OF STREAMS = 4

OSCILLATORY CASE
1/K(R) = 0.8000000E 01

CH(1) SIZE = 2 BY 2
0.41065899E 02 -0.17848561E 021
0.85063166E 01 -0.32902742E 011

0.11986747E 02 -0.40591970E 011
-0.13297591E 02 0.16840269E 011

CH(3) SIZE = 2 BY 2

CH(4) SIZE = 2 BY 2
0.29772104E 02 -0.48014827E 011
0.13175341E 02 -0.24403751E 011

0.29893397E 02 0.22108020E 011
-0.13452203E 02 0.12761046E 011

STEADY CASE

1/K(R) = 0.

CH(1) SIZE = 2 BY 2
0.81027073E 00 -0.81027073E 00
0.35425846E-00 -0.35425848E-00

0.33116364E-00 -0.33116364E-00

CH(3) SIZE = 2 BY 2

CH(4) SIZE = 2 BY 2
0.55431357E 00 -0.55431357E 00
0.26746202E-00 -0.26746202E-00

AERODYNAMIC INFLUENCES ON ELEMENTS BY SUPERSONIC STRIP THEORY

6

OSCILLATORY CASE
 $1/K(R) = 0.40000000E 01$

$\bar{W} = 0.24499999E 01$

NUMBER OF STRIPS = 4

CH(1) SIZE = 2 BY 2

0.61223587E 01	-0.39058710E 011	-0.62933545E 01	0.99004493E 001
0.15446437E 01	0.31125329E-001	-0.20665466E 01	-0.12606335E 011

CH(2) SIZE = 2 BY 2

0.31065251E 01	-0.27118593E 011	-0.51505253E 01	0.1118557E 001
0.19906042E 01	-0.44966330E-011	-0.22760270E 01	-0.74438580E 001

CH(3) SIZE = 2 BY 2

0.19321131E 01	0.13111043E 011	0.49905559E 01	0.6339735E 001
0.16069380E 01	-0.115225592E 001	-0.25059827E 01	-0.61761168E 001

CH(4) SIZE = 2 BY 2

0.43656130E 01	-0.10551950E 011	-0.43801361E 01	0.29555888E-001
0.20787904E 01	-0.13237961E-001	-0.21390743E 01	-0.23801012E-001

PUNCHED CARDS - NOS - H#10 - 24 THRU H#10 - 37

* DIRECT NUMERICAL INTEGRATION COEFFICIENTS BY SUPERSTRUCTURE STRATEGY

OSCILLATORY CASE

$1/k(r) = 0.80000000E 01$

$\pi = 0.25137789E 01$

$\text{NUMBER OF SHIFTS} = 4$

CH(1) SIZE = 2 BY 2	
0.25403119E 02	-0.78336976E 011
0.10494554E 02	-0.86506670E 001

-0.25574115E 02	0.19634566E 011
-0.11016458E 02	-0.16577762E 011

CH(2) SIZE = 2 BY 2	
0.10357052E 02	-0.72755752E 001

-0.10642475E 02	-0.11151575E 011
-----------------	------------------

CH(3) SIZE = 2 BY 2	
0.17530102E 02	-0.21065729E 011
0.88358944E 01	-0.33709711E-001

-0.17544626E 02	0.58752020E 001
-0.88961783E 01	-0.43284714E-001

NUMBER OF SHIFTS = 4

INFLUENTIAL INTRUSIVE CONTAMINANTS BY SUBSTRATE STRING THEORY

STEADY CASE

1/K(R) = 0.

NUMBER OF STRIPS = 4

CH(1) SIZE = 2 BY 2
0.47505847E-00 -0.47505847E-00
0.22051676E-00 -0.22051676E-00

CH(2) SIZE = 2 BY 2
0.20614082E-00 -0.20614082E-00

CH(3) SIZE = 2 BY 2
0.20614082E-00 -0.20614082E-00

CH(4) SIZE = 2 BY 2
0.32435972E-00 -0.32435972E-00
0.16648821E-00 -0.16648821E-00

ENHANCED CASES: 100% 40% THREE 30% 37%

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INPUT DATA

COSINE LAMBDA =	0.8000000E 00
B(R) =	0.64999999E 01
TAN LD =	0.7500000E 00
TAN TR =	-0.5000000E 00
C(1) =	0.8000000E 01

$$1/K = \frac{0.400000000E+01}{0.80000000E+01} = 0.$$

R = 0.15000000E-00

	$J_{31}(K)$	$J_{41}(K)$	$K_{11}(K)$	$K_{21}(K)$	$K_{31}(K)$	$L_{11}(K)$	$L_{21}(K)$
$0.74999999E-02$	$-0.27333333E-01$	$-0.26716665E-01$	$-0.23411999E-01$	$-0.20405366E-01$	$0.34833332E-01$	$0.17108332E-01$	$0.17108332E-01$
$0.31250000E-02$	$0.61115555E-02$	$0.31115555E-01$	$0.17166666E-01$	$0.94444444E-02$	$0.38043330E-02$	$0.38043330E-02$	$0.38043330E-02$

$$\text{WKB} = \frac{\text{OSCILLATORY CASE}}{0.40000000E+01}$$

$$1/K(R) = 0.40000000E 01$$

CH1 1) SIZE = 2 BY 2					
0.82001874E	01	-0.85972560E	011	-0.94911763E	01
-0.58696458E	01	0.73110541E	011	0.34727361E	01
CH2 2) SIZE = 2 BY 2					
0.14499702E	01	0.18151077E	011	-0.14196405E-00	-0.19130098E
-0.14499702E	01	0.18151077E	011	0.14196405E-00	-0.19130098E

CH(3) SIZE = 2 BY 2

```

CH( 4 ) SIZE = 2 BY 2
 0.60005280E 01 -0.19105424E 011   -0.60936828E 01  0.84950338E 001
 0.68430612E 00 -0.25560378E-001  -0.81209405E 00  0.10747413E-001

```

ALGORITHMIC INFLUENCE COEFFICIENTS BY SUPERSONIC STRIP THEORY

OSCILLATORY CASE

1/K(R) = 0.8000000E 01

X = 0.1799999E 01

NUMBER OF STRIPS = 4

CH(1) SIZE = 2 BY 2
 0.41085099E 02 -0.17848561E 021
 0.85083166E 01 -0.32902742E 011

CH(2) SIZE = 2 BY 2
 0.11960503E 02 -0.40507598E 011
 0.11960503E 02 -0.40507598E 011

CH(3) SIZE = 2 BY 2
 0.332479531E 02 -0.703597550E 021
 0.169123011E 02 -0.23939743E 021

CH(4) SIZE = 2 BY 2
 0.244600406E 02 -0.38357250E 021
 0.45326774E 01 -0.91177386E 001

PUNCHED CARDS NOS. 6010 THRU 65

ANALYTIC INFLUENCE COEFFICIENTS BY SUPERSONIC STRIKE THEORY

STEADY CASE

$1/K(R) = 0.$

M	0.1799999E 01
NUMBER OF STRIPS	4

CH(1) SIZE = 2 BY 2
 0.81027073E 00 -0.81027073E 00
 0.35425846E-00 -0.35425848E-00

CH(2) SIZE = 2 BY 2
 0.1799999E 01 -0.1799999E 00
 0.33042052E-00 -0.33042052E-00

CH(3) SIZE = 2 BY 2
 0.33042052E 00 -0.33042052E 00
 0.24628971E 00 0.24628971E-00

CH(4) SIZE = 2 BY 2
 0.45828220E-00 -0.45828220E-00
 0.94819973E-01 -0.94819972E-01

PUNCHED CARDS NOW FILED 66 THRU 71

AERODYNAMIC INFLUENCE COEFFICIENTS BY SUPERSONIC STRIP THEORY

3

OSCILLATORY CASE

$$1/K(R) = 0.80000000E 01$$

$$R = 0.71999999E 01$$

$$\text{NUMBER OF STRIPS} = 4$$

CH(1) SIZE = 2 BY 2

$$\begin{array}{cccc} 0.25403119E & 02 & -0.78336976E & 011 \\ 0.10494554E & 02 & -0.86506670E & 001 \end{array}$$

CH(2) SIZE = 2 BY 2

$$\begin{array}{cccc} 0.11111111E & 011 & -0.33333333E & 011 \\ 0.10357052E & 02 & -0.72755752E & 001 \end{array}$$

CH(3) SIZE = 2 BY 2

$$\begin{array}{cccc} 0.20000000E & 011 & -0.20000000E & 011 \\ 0.01111111E & 011 & -0.33333333E & 001 \end{array}$$

CH(4) SIZE = 2 BY 2

$$\begin{array}{cccc} 0.15526666E & 02 & -0.18542319E & 011 \\ 0.44747236E & 01 & -0.10564039E & -001 \end{array}$$

ADMITTED CARDS NO. 01 THRU 040 89

1. INFLUENCE COEFFICIENTS OF STATIONARY SHIP INERTIA

STEADY CASE

1/K(R) = 0.

= 0.7499999E 0

NUMBER OF STATIONS = 4

CH(1) SIZE = 2 BY 2
0.47505847E-00 -0.47505847E-00
0.22051676E-00 -0.22051676E-00

CH(2) SIZE = 2 BY 2
0.39560166E-00 -0.39560166E-00
0.20614082E-00 -0.20614082E-00

CH(3) SIZE = 2 BY 2
0.11998797E-00 -0.11998797E-00
0.11998226E-00 -0.11998226E-00

CH(4) SIZE = 2 BY 2
0.28739219E-00 -0.28739219E-00
0.84551580E-01 -0.84551579E-01

PRINTED CASES NO. 00 THRU 0010 95

B. Punched Output

1. A deck of punched cards (output) from this program is suitable as an input deck to other programs requiring the use of AICs.
2. All punched output is sequenced in order on Columns 73 through 80 starting with HM100000. The data appear in the following order:
 - a. Card 1 contains $(V/b_r \omega)_1$, and M_1 (FORMAT 6E12.8).
 - b. Card 2 contains m , the size (number of control points) of the AIC matrix and n , the number of strips (partitions) FORMAT (18I4).
 - c. The AIC matrix punched in column binary form and its TRA card make up the remainder of the punched output for $(V/b_r \omega)_1$.
3. The order of statement (2) is repeated for all Mach numbers and reduced velocities per input deck.
4. Each matrix is punched in compact form by columns. Column 1 begins in origin 1 and Column 2 in location (1 + matrix size).
5. The oscillatory matrix is punched in the order: Column 1 (real), Column 1 (imaginary); Column 2 (real), Column 2 (imaginary); Column m (real), Column m (imaginary). In the steady case, all columns are real and are punched in order.

SECTION V
PROCESSING INFORMATION

A. Operation

STANDARD FORTRAN MONITOR system

B. Estimated Machine Time

T = time in minutes

ISTRIP = number of strips

JMACH = number of Mach numbers

KVBRW = number of reduced velocities

n = number of sets (decks) of input data

$$T = .5 + .03 \left[(ISTRIP \cdot JMACH \cdot KVBRW)_1 + (ISTRIP \cdot JMACH \cdot KVBRW)_2 \right. \\ \left. + \dots + (ISTRIP \cdot JMACH \cdot KVBRW)_n \right]$$

C. Machine Components Used

Core storage: 6772

Standard FORTRAN input tape (NTAPE 2)

Standard FORTRAN output print tape (NTAPE 3)

Standard FORTRAN punch tape (NTAPE 7)

SECTION VI
PROGRAM NOTES

A. Subroutines Used

RDLN: reads and prints title cards

AEROP3: punch AIC matrix

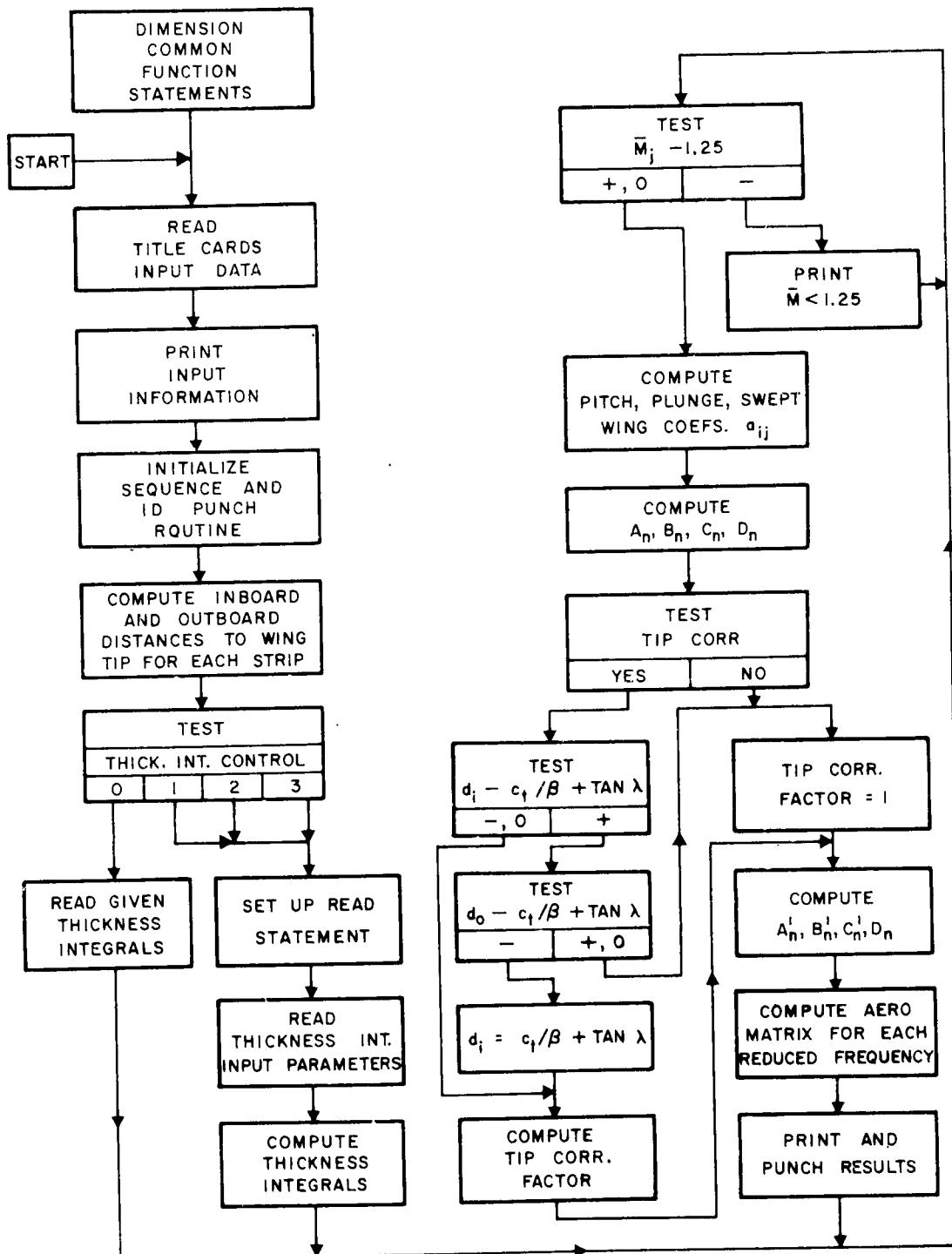
BINPU: column binary punch

All other subroutines used are on library tapes.

B. Generalized Tapes

Input, print, and punch tapes in this coding are defined as Units 2, 3, and 12 respectively; however, these may be altered by placing the desired units on symbolic cards HM100054, HM100055, and HM100056.

SECTION VII
FLOW DIAGRAM



SECTION VIII
SYMBOLIC LISTING

A partial list of the principal FORTRAN symbols used in the program may be related to the physical notation as follows:

<u>FORTRAN Notation</u>	<u>Physical Notation</u>
BI	b_i
DI	d_i
DELY	Δy
XMACHS	M_N
VBRW	$V/b_r \omega$
XMC	x_m/c
TAU	τ
AR	r
DISTO	d_o
DISTI	d_i
CHI	C_{h_i}
XLHO	L_{h_o}
XLAO	L_{a_o}
XMAO	M_{a_o}
XMHO	M_{h_o}
AI1, AI2, ..., AIN	I_1, I_2, \dots, I_n
AJ1, AJ2, ..., AJN	J_1, J_2, \dots, J_n
AK1, AK2, ..., AKN	K_1, K_2, \dots, K_n

SYMBOLIC LISTING (continued)

<u>FORTRAN Notation</u>	<u>Physical Notation</u>
AL1, AL2, ..., ALN	L_1, L_2, \dots, L_n
B	β
BB1, BB2, ..., BBN	B_1, B_2, \dots, B_n
C1, C2, ..., CN	C_1, C_2, \dots, C_n
D1, D2, ..., DN	D_1, D_2, \dots, D_n
FF1, FF2, ..., FFN	f_1, f_2, \dots, f_n
ISTRIP	Number of strips
JMACH	Number of Mach numbers
KVBRW	Number of reduced frequencies
ISTHK	Thickness integral control
ISTIP	Tip correction control
NO PUNJ	Punch control
BR	b_r
SMS	s
CAPS	S
CBAR	\bar{c}
CT	c_t
TANLA	$\tan \Lambda$
TANLAM	$\tan \lambda$
COSLA	$\cos \Lambda$

The complete symbolic listing is given on the following pages.

AERODYNAMIC INFLUENCES THEORY

```

      SUBROUTINE TAPESIZE(CASE)
      14 FORMAT ( 37H1 M BAR IS LESS THAN 1.25, M BAR =
      15 FORMAT (1HO 47X, 18H OSCILLATORY CASE )           1F6.3 )
      16 FORMAT (1HO 30X, 13H STEADY CASE )               HM100038
      17 FORMAT (1HO 31X, 15H SHOCK CASE )              HM100039
      18 FORMAT (1HO 44X, 3HCH1 112, 15H) SIZE = 2 BY 2   HM100040
      19 FORMAT (1H 36X, 2E17.8 )                         HM100041
      20 FORMAT (1H. 19X, 2E16.8,5H) 2E16.8, 1HI )        HM100042
      21 FORMAT (1H 36X, 2E17.8 )                         HM100043
      22 FORMAT (1H 36X, 2E17.8 )                         HM100044
      23 FORMAT (1H 36X, 2E17.8 )                         HM100045
      24 FORMAT (1H 36X, 2E17.8 )                         HM100046
      25 FORMAT (1H 36X, 2E17.8 )                         HM100047
      26 FORMAT (1H 36X, 2E17.8 )                         HM100048
      27 FORMAT (1H 36X, 2E17.8 )                         HM100049
      28 FORMAT (1H 36X, 2E17.8 )                         HM100050
      29 FORMAT (1H 36X, 2E17.8 )                         HM100051
      30 FORMAT (1H 36X, 2E17.8 )                         HM100052
      31 FORMAT (1H 36X, 2E17.8 )                         HM100053
      32 FORMAT (1H 36X, 2E17.8 )                         HM100054
      33 FORMAT (1H 36X, 2E17.8 )                         HM100055
      34 FORMAT (1H 36X, 2E17.8 )                         HM100056
      35 FORMAT (1H 36X, 2E17.8 )                         HM100057
      36 FORMAT (1H 36X, 2E17.8 )                         HM100058
      37 FORMAT (1H 36X, 2E17.8 )                         HM100059
      38 FORMAT (1H 36X, 2E17.8 )                         HM100060
      39 FORMAT (1H 36X, 2E17.8 )                         HM100061
      40 FORMAT (1H 36X, 2E17.8 )                         HM100062
      41 FORMAT (1H 36X, 2E17.8 )                         HM100063
      42 FORMAT (1H 36X, 2E17.8 )                         HM100064
      43 FORMAT (1H 36X, 2E17.8 )                         HM100065
      44 FORMAT (1H 36X, 2E17.8 )                         HM100066
      45 FORMAT (1H 36X, 2E17.8 )                         HM100067
      46 FORMAT (1H 36X, 2E17.8 )                         HM100068
      47 FORMAT (1H 36X, 2E17.8 )                         HM100069
      48 FORMAT (1H 36X, 2E17.8 )                         HM100070
      49 FORMAT (1H 36X, 2E17.8 )                         HM100071
      50 FORMAT (1H 36X, 2E17.8 )                         HM100072
      51 IF (ISTIP) 51,52,51
      52 WRITE OUTPUT TAPE NTAPE3, 5,
      53 GOTO. 53

```

AERODYNAMIC INFLUENCE COEFFICIENTS 4/05/62

```

52 WRITE OUTPUT TAPE NTAPE3, 6,          HM100076
53 WRITE OUTPUT TAPE NTAPE3, 7,          HM100077
54 WRITE OUTPUT TAPE NTAPE3, 8,          HM100078
      (CONTINUE K=1-10VERM)
55 DATA=0          HM100079
56 DO 54 I=1,ISTRIP          HM100080
54 ALONG=DELY(I)+ALONG          HM100081
      DISTO(I)=ALONG          HM100082
      DISTO(I)=ALONG          HM100083
55 DO 56 I=1,ISTRIP          HM100084
56 IF (ISTRIP-1) = 59,59,56          HM100085
      DISTO(ISTRIP)=0          HM100086
      IF (ISTRIP-1) = 59,59,56          HM100087
      DISTO(I)=DISTO(I-1)-DELY(I)          HM100088
      DISTO(ISTRIP)=0          HM100089
      IF (ISTRIP-1) = 59,59,56          HM100090
      DISTO(ISTRIP)=0          HM100091
      IF (ISTRIP-1) = 59,59,56          HM100092
      DISTO(ISTRIP)=0          HM100093
      IF (ISTRIP-1) = 59,59,56          HM100094
      DISTO(ISTRIP)=0          HM100095
      DISTO(ISTRIP)=0          HM100096
      DISTO(ISTRIP)=0          HM100097
      DISTO(ISTRIP)=0          HM100098
      JTAU=1          HM100099
      KCAMA=1          HM100100
      GOTO 68          HM100101
      IF (KCAMA=1) = 1          HM100102
      KCAMA=ISTRIP          HM100103
      KCAMA=ISTRIP          HM100104
      KCAMA=ISTRIP          HM100105
      KCAMA=ISTRIP          HM100106
      KCAMA=ISTRIP          HM100107
      KCAMA=ISTRIP          HM100108
      KCAMA=ISTRIP          HM100109
      KCAMA=1          HM100110
      GOTO 61          HM100111
      IXMC=1          HM100112
      IXMC=1          HM100113

```

```

      SUBROUTINE TAUJ(COEFFICIENTS)
      DATA JTAU,KGAMA/1,1/
      DO 67 K=1,JTAU
      I=1
      M=1
      IF (I>M) GOTO 66
      65 XMC3=XMC2*XMC(I)
      XMC2=XMC(I)
      N=R
      TAUK=TAU(K)
      ARE=1.0-AR(M)/(1.0-XMC(I))*(1.0-XMC(TAU))
      A11(K)=AR(M)*TAU(K)/2.0
      A12(K)=SOMEF(6.0,XMC(I)),ARE,2.0,-3.0*XMC(I),XMC3)
      ARE=1.0-AR(M)/(1.0-XMC(I))*(1.0-XMC(TAU))
      A13(K)=SOMEF(6.0,XMC(I)),ARE,3.0-6.0*XMC(I),XMC5)
      ARE=1.0-AR(M)/(1.0-XMC(I))*(1.0-XMC(TAU))
      A14(K)=SOMEF(6.0,XMC(I)),ARE,6.0-15.0*XMC(I),XMC6)
      ARE=1.0-AR(M)/(1.0-XMC(I))*(1.0-XMC(TAU))
      A15(K)=SOMEF(120.0,20.0-10.0*XMC(I))+XMC3,ARE,4.0-15.0*XMC(I),
     120.0*XMC2-10.0*XMC3,XMC5)
      ARE=1.0-AR(M)/(1.0-XMC(I))*(1.0-XMC(TAU))
      A16(K)=SOMEF(360.0,45.0-20.0*XMC(I))+XMC4,ARE,10.0-36.0*XMC(I),
     10.0*XMC5)
      66 CONTINUE
      67 CONTINUE
      END

```

4705762

```

145.0*XMC2-20.0*XMC3,XMC6)
AL1(K)=SOMEF(120.0,10.0-5.0*XMC2+2.0*XMC3,ARE,3.0-10.0*XMC(1),
AL2(K)=SOMEF(120.0,10.0-5.0*XMC2-2.0*XMC5)
AL3(K)=SOMEF(120.0,10.0-5.0*XMC2+2.0*XMC4,ARE,3.0-10.0*XMC(1),
AL4(K)=SOMEF(120.0,10.0-5.0*XMC2-2.0*XMC3)
CONTINUE

      WRITE(UNIT=13,FORMAT='(A$)')'THE LUMINESE COEFFICIENTS DUE TO FIGHT BUMBLE-GEE-SUE-E
      WRITE(UNIT=13,FORMAT='(A$)')'          (AJ1(K),AJ2(K),AJ3(K),AJ4(K),AK1(K),AK2(K),AK3(K))HM100163
      WRITE(UNIT=13,FORMAT='(A$)')'          ,AL1(K),AL2(K),K=1,JTAU)
      WRITE(UNIT=TAPE_NTAPE3, 13, '(AJ1(K),AJ2(K),AJ3(K),AJ4(K),AK1(K),AK2(K),AK3(K))HM100163
      ,AL1(K),AL2(K),K=1,JTAU)
      WRITE(UNIT=TAPE_NTAPE3, 14, 'EM
      GOTO 106

      END PROGRAM
      END SUBROUTINE
      END SUBROUTINE (4)COSLA
      IF (IER<=25) JI=71,71
      WRITE(UNIT=TAPE_NTAPE3, 14, 'EM
      GOTO 106

      END PROGRAM
      END SUBROUTINE
      END SUBROUTINE (4)COSLA
      A01=-4.0/B*COSLA
      A02=-4.0/B2*(EM2*EN-2.0)
      A11=8.0/B3*(2.0-EM2)*COSLA
      A12=8.0/B3*B3*B3
      A13=8.0/B3*B3*B3*B3
      A15=8.0/B4*((2.0-EM2)*(EM2+2.0)*COSLA
      A21=4.0/B5*((EM2+2.0)*COSLA
      A22=16.0/B3*B3
      HM100153
      HM100154
      HM100155
      HM100156
      HM100157
      HM100158
      HM100159
      HM100160
      HM100161
      HM100162
      HM100163
      HM100164
      HM100165
      HM100166
      HM100167
      HM100168
      HM100169
      HM100170
      HM100171
      HM100172
      HM100173
      HM100174
      HM100175
      HM100176
      HM100177
      HM100178
      HM100179
      HM100180
      HM100181
      HM100182
      HM100183
      HM100184
      HM100185
      HM100186
      HM100187
      HM100188
      HM100189
      HM100190

```

A B S O L U T E C O R R E C T I O N C O F F I C I E N T S		4/10/62
A23=8.0*EM2/B6*(3.0*(3.0*EM2-2.0)*EN-2.0*(5.0*EM2-3.0))		HM100190
A24=8.0*EM2/B4*(4.0*EN-5.0)		HM100191
A25=-.125*(.5*EM2*B6*(3.0*EN2-3.0))		HM100192
A26=-.125*(.5*EM2*B6*(3.0*EN2-3.0))		HM100193
A27=-.125*(.5*EM2*B6*(3.0*EN2-3.0))		HM100194
A28=-.125*(.5*EM2*B6*(3.0*EN2-3.0))		HM100195
A29=-.125*(.5*EM2*B6*(3.0*EN2-3.0))		HM100196
A30=-.125*(.5*EM2*B6*(3.0*EN2-3.0))		HM100197
A31=-8.0*EM2/(3.0*B6*B5*COSLA)		HM100198
A32=-24.0*EM2/B5*COSLA		HM100199
A33=16.0*EM2/B8*((17.0*EM2*EN2-10.0*EM2-4.0)*EN-(5.0*EM2		HM100200
-1.0)*EN)		
A34=8.0*EM2/B6*(2.0*(EM2+1.0)-(EM2+8.0)*EN)		HM100201
A35=8.0*EM2/B8*((3.0*EM2+2.0)-(3.0*EM2+4.0)*EN)		HM100202
A36=8.0*EM2/B6*((2.0*(EM2+1.0)-(EM2+8.0)*EN)		HM100203
A37=8.0*EM2/B8*((3.0*EM2+2.0)-(3.0*EM2+4.0)*EN)		HM100204
A38=-.125*(.5*EM2*B6*(3.0*EN2-3.0)-3.0*EN2*EN1)		HM100205
A39=-.125*(.5*EM2*B6*(3.0*EN2-3.0)-3.0*EN2*EN1)		HM100206
DO 72 I=1,J1AU		HM100207
A2(I)=-.125*(.5*A22+AJ1(I)*A24+A12(I)*A26)		HM100208
A3(I)=-.125*(A12+A11(I)*A14)		HM100209
A4(I)=.125*(.5*A22+AJ1(I)*A24+A12(I)*A26)		HM100210
A5(I)=.125*(.5*A22+AJ1(I)*A24+A12(I)*A26)		HM100211
A6(I)=.125*(.5*A22+AJ1(I)*A24+A12(I)*A26)		HM100212
A7(I)=.125*(.5*A22+AJ1(I)*A24+A12(I)*A26)		HM100213
A8(I)=.125*(.5*A22+AJ1(I)*A24+A12(I)*A26)		HM100214
B83(I)=.25*(.5*A11+AJ1(I)*A13+A12(I)*A15)		HM100215
B84(I)=.25*(.25*A31+A11(I)*A33+AK2(I)*A35+AJ3(I)*A37		HM100216
1+A14(I)*A39)		HM100217
C1(I)=.25*(.5*A22+AJ1(I)*A24+A12(I)*A26)		HM100218
C2(I)=.25*(.5*A22+AJ1(I)*A24+A12(I)*A26)		HM100219
D1(I)=.5*(.5*A01+A12(I)*A02)		HM100220
D2(I)=.5*(.25*A21+AK2(I)*A23+AJ3(I)*A25+A14(I)*A27)		HM100221
D3(I)=.5*(1.0/3.0*A11+AJ2(I)*A13+A13(I)*A15)		HM100222
D4(I)=.5*(1.0/3.0*A11+AJ2(I)*A13+A13(I)*A15)		HM100223
D5(I)=.5*(1.0/3.0*A11+AJ2(I)*A13+A13(I)*A15)		HM100224
END		HM100225
C TIP CORRECTION		HM100226
C .636619772 = 2/P1		HM100227
DO 90 I=1,ISTRIP		

C C O D E A N D I N F L U E N C E C O E F F I C I E N T S 4/28/85/62
 R13=RETA3/2.*(.5*DIST12*(1./TANL2-1./BETA2)+2./TANL3
 1.*CT*DIST1(I)-3./TANL4*CT2*TANL4*
 LOGEF(C100/CTDI)+CT3/TANL4*
 HM100304
 HM100305
 HM100306
 HM100307
 HM100308
 HM100309
 HM100310
 HM100311
 HM100312
 HM100313
 HM100314
 HM100315
 HM100316
 HM100317
 HM100318
 HM100319
 HM100320
 HM100321
 HM100322
 HM100323
 HM100324
 HM100325
 HM100326
 HM100327
 HM100328
 HM100329
 HM100330
 HM100331
 HM100332
 HM100333
 HM100334
 HM100335
 HM100336
 HM100337
 HM100338
 HM100339
 HM100340
 HM100341

C RMN COMMON
 B1 CONTINUE
 R10=.5*(2.*CT1*(DIST1(I))-DIST0(I))-(DIST12-DIST02)*(BETA+
 DIST1(I))
 R20=.5*(A2-TANL2-10*TANL1-I1-DIST0100*I10*TANL100*I101
 DIST13*(BETA13-015*TANL3)+BETA2*TANL2)
 R21=RETA11.0/73.0*(DIST13-DIST03)*(BETA+TANLAM)-.5*(DIST12
 1-DIST02)*CT1
 R30=1.0/12.0*(4.0*CT3*(DIST111)-DIST0(I))-6.0*CT2*TANLAM*
 DIST12-DIST02)*CT4*TANL2-DIST13-DIST03-1015*I14-DIST00*I10*
 DIST113
 R31=RETA11.0/73.0*(.25*(DIST14-DIST04)*(BETA2-TANL2)*
 1-DIST03)*CT*TANLAM-.5*(DIST12-DIST02)*CT2)
 R32=RETA2*(-.25*(DIST14-DIST04)*(BETA+TANLAM)+1.0/3.0*(DIST13
 1-DIST03)*CT1)
 R33=-.25*(DIST14-DIST04)*(BETA2-TANL2)*.25*(DIST12-DIST02)
 1-DIST03)*CT*TANLAM-10.0*(.25*(DIST14-DIST04)*(BETA2-TANL2)
 1-DIST03)*CT*TANLAM-1015*I12
 R41=RETA/3.*(.2*(DIST15-DIST05)*(BETA3+TANL3)-.75*(DIST14
 1-DIST04)*CT*TANL2+(DIST13-DIST03)*CT2*TANLAM-.5*(DIST12
 2-DIST02)*CT3)
 R42=-.25*(DIST14-DIST04)*(BETA2-TANL2)*.25*(DIST12-DIST02)
 1-DIST03)*CT*TANLAM-10.0*(.25*(DIST14-DIST04)*(BETA2-TANL2)
 1-DIST03)*CT*TANLAM-1015*I12
 R50=1.0/30.0*(6.0*CT5*(DIST11)-DIST0(I))-15.0*CT4*TANLAM*
 ((DIST12-DIST02)+20.0*CT3*TANL2*(DIST13-DIST03)-15.0*
 ((DIST14-DIST04)*CT1)

```

      SUBROUTINE INFLUENCE_COEFFICIENTS 4/06/62

      2CT12*TANL3*(DIST14-DIST04)+6.*C*CT*TANL4*(DIST15-DIST05)   HM100342
      3-(DIST16-DIST06)*(BETA5+TANL5)   HM100343
      C
      DIST14=0.5*(DIST15-BETAT15*TANL15-TANL15*BETAT15)   HM100344
      DIST15=0.5*(DIST14-BETAT14*TANL14-TANL14*BETAT14)   HM100345
      TANL15=0.5*(DIST15-BETAT15*TANL15)   HM100346
      TANL14=0.5*(DIST14-BETAT14*TANL14)   HM100347
      C
      R52=BETA2/3.*0*(-1.0/6.*0*(DIST16-DIST06)*(BETA3+TANL3)+*6* HM100348
      1(DIST15-DIST05)*CT*TANL2-*75*(DIST14-DIST04)*CT2*TANLAM   HM100349
      C
      DIST16=DIST15+DIST14+DIST13+DIST12+DIST11+DIST10+DIST09+DIST08+DIST07+DIST06+DIST05+DIST04+DIST03+DIST02+DIST01+DIST00   HM100350
      C
      R51=0.5*(DIST16+0.5*(DIST15+0.5*(DIST14+0.5*(DIST13+0.5*(DIST12+0.5*(DIST11+0.5*(DIST10+0.5*(DIST09+0.5*(DIST08+0.5*(DIST07+0.5*(DIST06+0.5*(DIST05+0.5*(DIST04+0.5*(DIST03+0.5*(DIST02+0.5*(DIST01+0.5*(DIST00))))))))))))))))   HM100351
      C
      RMN FOR LAMBDA = 0   HM100352
      C
      C    RMN FOR SMALL VALUE OF LAMBDA   HM100353
      C
      HZ_Coeffines   HM100354
      DIST17=0.5*(DIST16+DIST15)   HM100355
      DIST18=0.5*(DIST14+DIST13)   HM100356
      DIST19=0.5*(DIST12+DIST04+DIST03)   HM100357
      DIST20=0.5*(DIST11+DIST09+DIST08+DIST07)   HM100358
      DIST21=0.5*(DIST10+DIST06+DIST05+DIST04+DIST03+DIST02+DIST01+DIST00)   HM100359
      C
      RAT1=(DIST11(1)-DIST01(1))/CT1   HM100360
      RAT2=(DIST12-DIST02)/CT2   HM100361
      RAT3=(DIST13-DIST03)/CT3   HM100362
      RAT4=(DIST14-DIST04)/CT4   HM100363
      RAT5=(DIST15-DIST05)/CT5   HM100364
      RAT6=(DIST16-DIST06)/CT6   HM100365
      RAT7=(DIST17-DIST07)/CT7   HM100366
      RAT8=(DIST18-DIST08)/CT8   HM100367
      RAT9=(DIST14*DIST15-DIST04*DIST05)/(CT4*CT5)   HM100368
      C
      RAT10=(DIST11(2)-DIST01(2))/CT1   HM100369
      RAT11=(DIST12(2)-DIST02(2))/CT2   HM100370
      RAT12=(DIST13(2)-DIST03(2))/CT3   HM100371
      RAT13=(DIST14(2)-DIST04(2))/CT4   HM100372
      RAT14=(DIST17*DIST17-DIST07*DIST07)/(CT7*CT7)   HM100373
      RAT15=(DIST17*DIST18-DIST07*DIST08)/(CT7*CT8)   HM100374
      C

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THE JOURNAL OF CLIMATE

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        SUBROUTINE DISTANCE COEFFICIENTS 4/06/62

R33=.25*BETA3*(DIST04*LOGEF(CTD0/(BETA*DIST0(1)))-DIST14*
1LOGEF(CTD1/(BETA*DIST1(1)))-CT4*(.25*RAT4+TANLAM/5.0*RAT5+
.25*RAT6+TANLAM/6.0*RAT7+.25*RAT8+TANLAM/7.0*RAT9+.25*RAT10+
.25*RAT11+TANLAM/11.0*RAT12+.25*RAT13+TANLAM/13.0*RAT14+
.25*RAT15+TANLAM/15.0*RAT16+.25*RAT17+TANLAM/17.0*RAT18+
.25*RAT19+TANLAM/19.0*RAT20+.25*RAT21+TANLAM/21.0*RAT22+
.25*RAT23+TANLAM/23.0*RAT24+.25*RAT25+TANLAM/25.0*RAT26)
GOTO 81

84 CONTINUE

R12=BETA2*(.5/BETA*DIST12-CT2*(1./3.*RAT3+TANLAM/4.*RAT4+
1RAT4+TANL2/5.*RAT5+TANL3/6.*RAT6+TANL5/7.*RAT7+TANL5/
10.*RAT8+TANL9/11.*RAT11))
3TANL8/10.*RATIO+TANL9/11.*RAT11)
3TANL7/12.*RATIO+TANL8/13.*RAT12)
3TANL6/15.*RATIO+TANL7/16.*RAT13)
3TANL5/20.*RATIO+TANL6/21.*RAT14)
3TANL4/25.*RATIO+TANL5/26.*RAT15)
3TANL3/30.*RATIO+TANL4/31.*RAT16)
3TANL2/35.*RATIO+TANL3/36.*RAT17)
3TANL1/40.*RATIO+TANL2/41.*RAT18)
3TANL0/45.*RATIO+TANL1/46.*RAT19)
3TANL7/10.*RATIO+TANL8/11.*RAT11+TANL9/12.*RAT12)
R23=BETA3*(-1./(13.*BETA)*DIST13+CT3*(.25*RAT4+TANLAM/5.0*
1.RAT5+TANL2/6.*RAT6+TANL3/7.*RAT7+TANL4/8.*KAT8+TANL5/9.*KAT9+
.25*RAT10+TANL6/10.*RAT11+TANL7/11.*RAT12+TANL8/12.*RAT13+
.25*RAT14+TANL9/14.*RAT15+.25*RAT15+TANL10/15.*RAT16+
.25*RAT16+TANL11/16.*RAT17+.25*RAT17+TANL12/17.*RAT18+
.25*RAT18+TANL13/18.*RAT19+.25*RAT19+TANL14/19.*RAT20+
.25*RAT20+TANL15/20.*RAT21+.25*RAT21+TANL16/21.*RAT22+
.25*RAT22+TANL17/22.*RAT23+.25*RAT23+TANL18/23.*RAT24+
.25*RAT24+TANL19/24.*RAT25+.25*RAT25+TANL20/25.*RAT26)
GOTO 81

CONTINUE
Q1=E *R10+E1*R11+E2*R12+E3*R13
Q2=E *R20+E1*R21+E2*R22+E3*R23
Q3=E *R30+E1*R31+E2*R32+E3*R33

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      SUBROUTINE INTRUECT_COTIENTS  A706767

Q4=E *R40+E1*R41+E2*R42+E3*R43
HM100456
Q5=E *R50+E1*R51+E2*R52+E3*R53
HM100457
HM100458
HM100459
HM100460
HM100461
HM100462
HM100463
HM100464
HM100465
HM100466
HM100467
HM100468
HM100469
HM100470
HM100471
HM100472
HM100473
HM100474
HM100475
HM100476
HM100477
HM100478
HM100479
HM100480
HM100481
HM100482
HM100483
HM100484
HM100485
HM100486
HM100487
HM100488
HM100489
HM100490
HM100491
HM100492
HM100493

Q4=E *R40+E1*R41+E2*R42+E3*R43
Q5=E *R50+E1*R51+E2*R52+E3*R53
FF3=1.-375/18(I)**3*DELY(I)*(Q3+2.*EEE*Q2+EEE*Q1)
FF4=1.-25/(B(I)**64*DELY(I))*(Q4+3.*EEE*Q3+3.*EEE*EEE)*Q2+
1.EEE*(EEE*EEE)*Q1
IF (JTAU-ISTRIP) 89,88,89
86 L=I
IF (JTAU-ISTRIP) 89,88,89
88 L=I
A4(I)=FF3*A4(I)
BB1(I)=FF1*BB1(I)
BR2(I)=FF3*BB2(I)
C3(I)=FFF2*C3(I)
C4(I)=FFF4*C4(I)
D1(I)=FF2*D1(I)
D2(I)=FF3*D2(I)
D3(I)=FF4*D3(I)
D4(I)=FFF5*D4(I)
CONTINUE
90 CONTINUE
91 DO 105 K=1,KVBRW
      C1=1.0
      C2=1.0
      C3=1.0
      C4=1.0
      D1=1.0
      D2=1.0
      D3=1.0
      D4=1.0
      GOTO 94
93 WRITE OUTPUT TAPE NTAPE3, 16

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94 WRITE OUTPUT TAPE NTAPE3, 17, VBRW(K), XMACHS(J),ISTRIP
      HML00494
      HML00495
      HML00496
      HML00497
      HML00498
      HML00499
      HML00500
      HML00501
      HML00502
      HML00503
      HML00504
      HML00505
      HML00506
      HML00507
      HML00508
      HML00509
      HML00510
      HML00511
      HML00512
      HML00513
      HML00514
      HML00515
      HML00516
      HML00517
      HML00518
      HML00519
      HML00520
      HML00521
      HML00522
      HML00523
      HML00524
      HML00525
      HML00526
      HML00527
      HML00528
      HML00529
      HML00530
      HML00531

      DO 103 I=1,ISTRIP
      IF (VBRW(K)) 97,97,98
      OSCILLATORY AERODYNAMIC COEFFICIENTS-STEADY CASE
      103 XLAO(2)=0.
      XMHO(1)=0.
      XMHO(2)=0.
      CAY=C2(1)
      XMHO(1)=C3(1)/CAY+C4(1)*CAY
      XMHO(2)=RB3(1)/CAY+BB4(1)*CAY
      CH(1,N+2,I)=EX*(-.5*ZEE*WHY*XLAO(N)+.5*(ZEE**2)*XMHO(N)**ZEE*WHY
      1   XMHO(N)-ZEE**2*XMAO(N))
      1   CH(2,N+1,I)=EX*(-.5*ZEE*WHY*XLAO(N)+ZEE*WHY*XMHO(N)+.5*(ZEE**2)
      1   *CH(1,N+2,I))
      GOTO 99
      98 CAY=B1(1)/(VBRW(K)*BR)
      99 ZEE=BT(1)/DI(1)
      WHY=1.0+.5*ZEE
      END

```


ALTERED INSTRUCTION COUNTS - 8/106/62

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STORAGE NOT USED BY PROGRAM

DEC	OCT	DEC	OCT
DEC	OCT	DEC	OCT
A11 32361 77151	AK2 32356 77120	A13 32361 77067	AI1 32361 76641
A15 32356 76619	AI1 32111 76457	AI2 32366 76576	AI3 32368 76475
AJ4 32211 76723	AK1 32186 76672	AR 32286 77036	BI 32561 77461
CH 32036 76444	DELY 32511 77377	DI 32536 77430	DIST 32236 76754
DISTO 32261 77005	TAU 32386 77202	VBRW 32461 77315	XMAHS 32486 77346
ARE 32311 77233			

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON STATEMENTS

DEC	OCT	DEC	OCT
DEC	OCT	DEC	OCT
A2 5408 12440	A3 5333 12325	A4 5258 12212	AK2 5433 12471
A63 53318 12356	AI1 5203 12243	AI2 5103 12077	AI3 5093 11732
B82 50608 11620	AI3 5013 11505	BB1 4908 11555	C2 5233 12161
C3 5113 12015	AI4 5013 11521	BI 5158 12046	D2 5058 11702
D3 4983 11567	D4 4958 11536	XLA0 5308 12274	XLR0 5383 12407
XMA0 5108 11764	XMM0 5208 12130		

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN DIMENSION AND EQUIVALENCE STATEMENTS

DEC	OCT	DEC	OCT
DEC	OCT	DEC	OCT
A01 4883 11423	A02 4882 11422	AI1 4881 11421	AI2 4880 11420
A13 4879 11417	A14 4878 11416	A15 4877 11415	A21 4876 11414
A22 4875 11413	A23 4874 11412	A24 4873 11411	A25 4872 11410
A26 4871 11407	A27 4870 11406	A28 4869 11405	A32 4868 11404
A31 4867 11403	A32 4866 11402	A33 4865 11401	A36 4864 11400
A37 4863 11377	A38 4862 11376	A39 4861 11375	A40 4860 11374
ARE 4859 11373	B2 4858 11372	B3 4857 11371	B4 4856 11370
B5 4855 11367	B6 4854 11366	B8 4853 11365	BETA2 4852 11364
BETA3 4851 11363	BETA4 4850 11362	BETAS 4849 11361	BETA 4848 11360
BE 4857 11357	BE1 4856 11356	BE2 4855 11355	CAT 4854 11354

AERODYNAMIC COEFFICIENTS										4/06/62	
CBAR	4843	11353	COSLA	4842	11352	CT2	4841	11351	CT3	4840	11350
CT4	4839	11347	CT5	4838	11346	CT6	4837	11345	CT7	4836	11344
CT8	4836	11343	CT9	4835	11342	GFO	4833	11341	CT1	4832	11340
D112	4811	11337	DIST12	4830	11336	DIST13	4829	11335	DIST14	4828	11334
D1515	4817	11333	DIST16	4826	11332	DIST17	4825	11331	DIST18	4824	11330
D15102	4823	11327	DIST03	4822	11326	DIST04	4821	11325	DIST05	4820	11324
D15106	4819	11323	DIST07	4818	11322	DIST08	4817	11321	E1	4816	11320
E2	4815	11317	E3	4814	11316	EEE	4813	11315	EM2	4812	11314
EN	4811	11311	EN	4810	11312	E	4809	11311	EX	4808	11310
E1	4807	11307	E2	4806	11306	E1	4805	11305	E2	4804	11304
FF3	4803	11303	FF4	4802	11302	E3	4801	11301	GAMA	4800	11300
I	4799	11277	ISTHK	4798	11276	ISTIP	4797	11275	ISTRIP	4796	11274
IXMC	4795	11273	JMACH	4794	11272	JTAU	4793	11271	JTWO	4792	11270
KGAMA	4791	11267	K	4790	11266	KVBRW	4789	11265	L	4788	11264
M	4787	11263	NUARDS	4786	11262	NURUNI	4785	11261	NURUT2	4784	11260
N1API3	4783	11257	NIAH17	4782	11256	O1	4781	11255	O2	4780	11254
O3	4779	11253	O4	4778	11252	O5	4777	11251	O10	4776	11250
R11	4775	11247	R12	4774	11246	R13	4773	11245	R20	4772	11244
R21	4771	11243	R22	4770	11242	R23	4769	11241	R30	4768	11240
R31	4767	11237	R32	4766	11236	R33	4765	11235	R40	4764	11234
R41	4763	11233	R42	4762	11232	R43	4761	11231	R50	4760	11230
R51	4759	11229	R52	4758	11228	R53	4757	11225	R610	4756	11224
R611	4755	11225	R612	4754	11222	R613	4753	11221	R614	4752	11220
R615	4751	11217	RAT1	4750	11216	RAT2	4749	11215	RAT3	4748	11214
RAT4	4747	11213	RAT5	4746	11212	RAT6	4745	11211	RAT7	4744	11210
RAT8	4743	11207	RAT9	4742	11206	SAVE	4741	11205	SMS	4740	11204
TANH10	4739	11203	TANH11	4738	11202	TAN12	4737	11201	TANH13	4736	11200
TANH14	4735	11177	TANH15	4734	11176	TAN16	4733	11175	TANH17	4732	11174
TANL4	4730	11173	TANL5	4730	11172	TANL6	4729	11171	TANL7	4728	11170
TANL8	4727	11167	TANL9	4725	11166	TANLAM	4725	11165	TANLA	4724	11164
TAUK	4723	11163	WHY	4722	11162	XMC2	4721	11161	XMC3	4720	11160
XMC4	4719	11157	XMC5	4718	11156	XMC6	4717	11155	ZEE	4716	11154

SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM STATEMENTS

AERODYNAMIC INFLUENCE COEFFICIENTS - 4/1966/62

	EFN	LOC	EFN	LOC	EFN	LOC	EFN	LOC			
1) S	13	10531	2) E	11195	3) S	11196	4) S	11197			
2) S	13	10612	3) S	10531	5) S	10531	6) S	10530			
3) S	13	10531	4) E	10560	6) S	10531	7) C	10530			
4) D	13	10612	5) E	14	8) F	15	10546	8) G	16	10537	
5) H	17	10531	6) I	18	10507	8) J	19	10477	8) K	20	10473

ROUTINES FOR COMPUTING INVERSE FUNCTIONS

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
1) AERO3	10	00012	ATAN	9 00011	EXP(3	8 00010	LOG	1 00001
2) S	385	00601	SQRT	9 00011	F1L1	6 00000	F1P1	0 00000
3) R	1475	02703	RDLN	9 00011	F1L2	6 00000	F1P2	3 00000
4) S	1300	10531	SQRT	9 00011	F1L3	6 00000	F1P3	3 00000

ROUTINES FOR COMPUTING INVERSE FUNCTIONS

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
1) AERO3	10	00012	ATAN	9 00011	EXP(3	8 00010	LOG	1 00001
2) S	385	00601	SQRT	9 00011	F1L1	6 00000	F1P1	0 00000
3) R	1475	02703	RDLN	9 00011	F1L2	6 00000	F1P2	3 00000
4) S	1300	10531	SQRT	9 00011	F1L3	6 00000	F1P3	3 00000

ENTRY POINTS TO SUBROUTINES NOT OUTPUT FROM LIBRARY

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
1) AERO3	10	00012	ATAN	9 00011	EXP(3	8 00010	LOG	1 00001
2) S	385	00601	SQRT	9 00011	F1L1	6 00000	F1P1	0 00000
3) R	1475	02703	RDLN	9 00011	F1L2	6 00000	F1P2	3 00000
4) S	1300	10531	SQRT	9 00011	F1L3	6 00000	F1P3	3 00000

ROUTINES FOR COMPUTING FINITE ELEMENT FUNCTIONS

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
1) AERO3	10	00012	ATAN	9 00011	EXP(3	8 00010	LOG	1 00001
2) S	385	00601	SQRT	9 00011	F1L1	6 00000	F1P1	0 00000
3) R	1475	02703	RDLN	9 00011	F1L2	6 00000	F1P2	3 00000
4) S	1300	10531	SQRT	9 00011	F1L3	6 00000	F1P3	3 00000

EQUITY EFFICIENCIES 6/06/02

	EFN	LOC	FFN	LOC	EFN	LOC	FFN	LOC	EFN	LOC	FFN	LOC
8)D	13	10612	8)E	14	10560	8)F	15	10546	8)G	16	10537	8)H
8)H	17	10531	8)I	18	10507	8)J	19	10477	8)K	20	10473	

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AEROP 3							
	DEC	OCT	ATAN	DEC	OCT	EXP(3	OCT
10	00012	9	00011	11111	11111	8	000010
				11111	11111	6	000000
				11111	11111	5	000000
				11111	11111	4	000000
				11111	11111	3	000000
				11111	11111	2	000000
				11111	11111	1	000000
				11111	11111	0	000000

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STATEMENT FUNCTIONS

AERODYNAMIC INFLUENCE COEFFICIENTS 4/06/62

LOGUE 4332 10354 DEC 4337 10361 DEC OCT

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

	EFN	IFN	LNC	EFN	IFN	LNC	EFN	IFN	LNC	EFN	IFN	LNC	EFN	IFN	LNC
50	32	00032	51	69	00236		52	72	00244	53	74	00250			
54	86	00312	55	91	00331		56	95	00354	57	96	00361			
58	102	00430	59	106	00437		60	110	00446	61	113	00454			
64	147	00602	66	148	00606		67	170	01312	68	171	01402			
70	184	01474	71	187	01507		72	234	02534	73	237	02551			
74	243	02564	75	253	02677		76	254	02705	77	255	02707			
78	279	03030	79	280	03032		80	288	03537	81	295	04123			
82	311	03117	83	346	05364		84	354	06313	85	362	07142			
86	374	07475	88	376	07505		89	377	07511	90	391	07563			
91	392	07510	92	395	07607		93	397	07616	94	398	07624			
97	403	07671	98	413	07717		99	423	0022	100	430	10177			
101	435	10226	102	438	10250		103	445	10275	104	447	10321			
105	449	10344	106	450	10350										

STORAGE NOT USED BY PROGRAM

DEC	OCT	DEC	OCT
HEX		HEX	
011	00011	012	00012
16	00010	32	00010

SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

HEX	LOC	HEX	LOC	HEX	LOC
DEC	OCT	DEC	OCT	DEC	OCT
011	00011	012	00012	013	00013
32	00010	64	00110	111	200034

LOCATIONS FOR OTHER SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	OCT	DEC	OCT	DEC	OCT
HEX		HEX		HEX	
61	00011	62	00010	63	00011
128	02000	129	02001	130	02002

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
HEX		HEX		HEX		HEX	
(FIL)	3 00003	(RTN)	1 00001	(STH)	2 00002	(TSH)	0 00000
(FIL)	4 00004	(RTN)	5 00005	(STH)	6 00006	(TSH)	7 00007

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

HEX	LOC	HEX	LOC	HEX	LOC	HEX	LOC
DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
011	00011	012	00012	013	00013	014	00014
32	00010	64	00110	111	200034	112	200035

STORAGE NOT USED BY PROGRAM

DEC	101
OCT	1001
BIN	001111

NOT USED

STORAGE LOCATIONS FOR VARIABLES APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENTS

DEC	31
OCT	37
BIN	11110

A

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN COMMON, DIMENSION, OR EQUIVALENCE STATEMENTS

DEC	101
OCT	1001
BIN	001111

NOT USED

DEC	200
OCT	240
BIN	10000000

DEC	201
OCT	241
BIN	10000001

DEC	202
OCT	242
BIN	10000010

DEC	203
OCT	243
BIN	10000011

DEC	204
OCT	244
BIN	10000100

DEC	205
OCT	245
BIN	10000101

DEC	206
OCT	246
BIN	10000110

DEC	207
OCT	247
BIN	10000111

DEC	208
OCT	248
BIN	10001000

DEC	209
OCT	249
BIN	10001001

DEC	210
OCT	250
BIN	10001010

DEC	211
OCT	251
BIN	10001011

DEC	212
OCT	252
BIN	10001100

DEC	213
OCT	253
BIN	10001101

DEC	214
OCT	254
BIN	10001110

DEC	215
OCT	255
BIN	10001111

DEC	216
OCT	256
BIN	10010000

DEC	217
OCT	257
BIN	10010001

DEC	218
OCT	258
BIN	10010010

DEC	219
OCT	259
BIN	10010011

DEC	220
OCT	260
BIN	10010100

DEC	221
OCT	261
BIN	10010101

DEC	222
OCT	262
BIN	10010110

DEC	223
OCT	263
BIN	10010111

DEC	224
OCT	264
BIN	10011000

DEC	225
OCT	265
BIN	10011001

DEC	226
OCT	266
BIN	10011010

DEC	227
OCT	267
BIN	10011011

DEC	228
OCT	268
BIN	10011100

DEC	229
OCT	269
BIN	10011101

DEC	230
OCT	270
BIN	10011110

DEC	231
OCT	271
BIN	10011111

SYMBOLS AND LOCATIONS FOR SOURCE PROGRAM FORMAT STATEMENTS

EN	1006
OT	1007
BN	1008

NOT USED

EN	1009
OT	1010
BN	1011

NOT USED

EN	1012
OT	1013
BN	1014

NOT USED

EN	1015
OT	1016
BN	1017

NOT USED

EN	1018
OT	1019
BN	1020

NOT USED

EN	1021
OT	1022
BN	1023

NOT USED

EN	1024
OT	1025
BN	1026

NOT USED

EN	1027
OT	1028
BN	1029

NOT USED

EN	1030
OT	1031
BN	1032

NOT USED

EN	1033
OT	1034
BN	1035

NOT USED

EN	1036
OT	1037
BN	1038

NOT USED

EN	1039
OT	1040
BN	1041

NOT USED

EN	1042
OT	1043
BN	1044

NOT USED

EN	1045
OT	1046
BN	1047

NOT USED

EN	1048
OT	1049
BN	1050

NOT USED

EN	1051
OT	1052
BN	1053

NOT USED

EN	1054
OT	1055
BN	1056

NOT USED

EN	1057
OT	1058
BN	1059

NOT USED

EN	1060
OT	1061
BN	1062

NOT USED

LOCATIONS OF NAMES IN TRANSFER VECTOR

EN	1063
OT	1064
BN	1065

NOT USED

EN	1066
OT	1067
BN	1068

NOT USED

EN	1069
OT	1070
BN	1071

NOT USED

EN	1072
OT	1073
BN	1074

NOT USED

EN	1075
OT	1076
BN	1077

NOT USED

EN	1078
OT	1079
BN	1080

NOT USED

EN	1081
OT	1082
BN	1083

NOT USED

EN	1084
OT	1085
BN	1086

NOT USED

EN	1087
OT	1088
BN	1089

NOT USED

EN	1090
OT	1091
BN	1092

NOT USED

EN	1093
OT	1094
BN	1095

NOT USED

EN	1096
OT	1097
BN	1098

NOT USED

EN	1099
OT	1100
BN	1101

NOT USED

EN	1102
OT	1103
BN	1104

NOT USED

EN	1105
OT	1106
BN	1107

NOT USED

EN	1108
OT	1109
BN	1110

NOT USED

EN	1111
OT	1112
BN	1113

NOT USED

EN	1114
OT	1115
BN	1116

NOT USED

BINPU		(FIL)		(STH)		INTERVALS AND FREQUENCIES								
		EFN	IFN	LDC	EFN	IFN	LDC	EFN	IFN	LDC	EFN	IFN	LDC	
4	12 00055	5	13 00057	6	22 00120	7	29 00207							
8	35 00232	9	37 00242	10	39 00253	11	40 00271							

CHIPPING ROUTINE TO WRITE OUT SIX CARDS ON TAPE, FINI

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00016	0402	00 0	00325	SUB	01		HM100652
00017	0622	30 0	00066	STD	LOCN		HM100653
00018	0012	00 0	00001	STO	COLN+0		HM100654
00019	0000	00 0	00000	STO	0		HM100655
00020	0000	00 0	00000	STO	1		HM100656
00021	0000	00 0	00000	STO	2		HM100657
00022	0711	00 0	00001	STO	3		HM100658
00023	-0120	00 0	00325	TWI	*+2	ADD RELATIVE BIT	HM100659
00024	-0501	00 0	00266	ORA	REL	7-9, WORD COUNT=22	HM100660
00025	-0501	00 0	00324	ORA	IMAGE	WORD COUNT IS 16	HM100661
00026	0002	00 0	00000	SET	CHANGE	CONTROL WORD ESTABLISHED	HM100662
00027	0114	00 2	000002	SET	0	TEST FOR WORD COUNT IS 16	HM100663
00028	0020	00 0	000002	SET	0	SET BLANK TO ITS NORMAL STATE	HM100664
00029	-0500	00 0	00000	END	0	TEST FOR 4TH ARGUS	HM100665
00030	-0500	00 0	00000	END	0		HM100666
00031	-0500	00 0	00000	ANA	FSKPDT		HM100667
00032	-0320	00 0	00265	FRA	MSKISX	NO MORE TSXES	HM100668
00033	0322	00 0	00307	TNZ	G2		HM100669
00034	-0100	00 0	00054	STZ	0	THIS IS 10	HM100670
00035	0000	00 0	00000	STZ	0	EQUAL, FLAG BLANK SEQ. NO.	HM100671
00036	-0100	00 0	00001	STZ	0	IS SEQ NO NON-ZERO.	HM100672
00037	0000	00 0	00001	STZ	0	NO	HM100673
00038	0000	00 0	00000	STZ	0	SMALL, THIS IS SEQ NO.	HM100674
00039	0000	00 0	00000	STZ	0		HM100675
00040	0600	00 0	00302	STZ	0		HM100676
00041	-0100	00 0	00043	TNZ	*+2		HM100677
00042	-0754	00 0	00000	PXD			HM100678
00043	-0110	00 0	00000	RET			HM100679
00044	0032	00 0	00000	RET			HM100680
00045	0074	00 0	00172	CONT	0	CONTINUE SEQ NO TO END	HM100681
00046	0774	00 4	00000	AXT	*+4		HM100682
00047	0602	00 0	00267	SLW	SEQNO	SAVE	HM100683
00048	177777	4 00053		TX1	G5,*4,-1		HM100684
00049	0001	00 0	00000	STO	00010	MOVE TO HIGH ADDRESS	HM100685
00050	177777	4 00053		END	00000-1	AT LAST 2 EXTRA ARGUS.	HM100686
00051	200001	2 00031		END	00024-1		HM100687
00052	0634	00 4	00144	G2	SXA	IS WORD COUNT ZERO	HM100688
00053	-0520	00 0	77776	NZ	FND	MUST BE A TRANSFER CARD	HM100689
00054	0020	00 0	00152	TRA	TRCD		

BUILD THE TWO IMAGE

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***** BUILD THE TWO IMAGE *****

00057 0774 00 2 00026 NEXT AXI 22,2
00060 -0754 00 0 00000 PXD
00061 0774 00 4 00000 COUNT AXI ***,4
***** BUILD THE TWO IMAGE *****

00062 0000 00 1 00000 INSET LOS TXI
00063 0000 00 2 77710 TXI
00064 0001 00 2 77710 TXI
00065 1 00001 4 00066 LOCN TXI
00066 3 00000 4 00160 L0CN TXI
00067 2 00001 2 00062 TIX
00070 0020 00 * 00001 IN TXI
00071 0001 00 0 00000 TXI
00072 0002 00 0 77761 TXI
***** BUILD THE TWO IMAGE *****

00073 0000 00 0 00267 EDIT CHI 22,2
00074 0560 00 0 00327 LDQ [1]
00075 -0765 00 0 00022 LGR 18
00076 -0500 00 0 00305 CAL BC0ID
00077 -0763 00 0 00000 LSC 6
00078 -0760 00 0 00000 SHI 10
00079 -0760 00 0 00000 SHI 10
00080 0174 00 0 00000 SHI 10
00081 -0739 00 0 00000 SHI 10
00102 0634 00 1 00120 SXA SV1,1
00103 0774 00 2 00004 AXI 4,2
00104 0774 00 4 00002 AXI 2,4
00105 0175 00 0 00003 SHI 11
00106 0175 00 0 00000 SHI 11
00107 0175 00 0 00000 SHI 11
00110 -2 00001 1 00113 TNX **3,1,1
00111 0767 00 0 00014 ALS 12
00112 0020 00 0 00107 TRA *-3
***** BUILD THE TWO IMAGE *****

HM100690
HM100695
HM100696
HM100697
HM100698
HM100699
HM100700
HM100701
HM100702
HM100703
HM100704
HM100705
HM100706
HM100707
HM100708
HM100709
HM100710
HM100711
HM100712
HM100713
HM100714
HM100715
HM100716
HM100717
HM100718
HM100719
HM100720
HM100721
HM100722
HM100723
HM100724
HM100725
HM100726
HM100727

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***** MM100766 ***** MM100767 *****
00151 0020 00 0 00057  TRA   NEXT
***** MM100768 ***** MM100769 *****
00152 00153 00 2 00001  TRA   REST OF
00153 00002 00 2 00001  TRA   CARD IMAGE.
00154 2 00001 2 00153  TIX   *-1,2,1
00155 0500 00 0 00322  CLA   ZWC
00156 0622 00 0 77740  STD   CIMAGE
00157 00002 00 0 00013  TIX   EBIT
00158 00002 00 0 00013  TIX   CIMAGE
00159 00002 00 0 00013  TIX   CIMAGE
00160 0600 00 0 77776  OUT  WORD COUNT EXHAUSTED
00161 -2 00001 2 00070  TNX  RETURN IF CARD IS FULL
00162 00002 00 0 00013  TIX   SAVE CHECKSUM.
00163 -00002 00 2 00000  CAL  COMMUN
00164 00002 00 0 77740  STD  CIMAGE
00165 0622 00 0 77740  STD  CIMAGE
00166 -0500 00 0 77777  CAL  COMMUN
00167 -3 00000 2 00070  TXL  IN,2,0
00168 00002 00 2 77779  TIX  CIMAGE
00169 00002 00 2 77779  TIX  CIMAGE
00170 00002 00 2 77779  TIX  CIMAGE
00171 00002 00 2 77779  TIX  CIMAGE
00172 -0153 00 0 00000  TIX   TEST IF CHARACTERS DESIRED.
00173 00002 00 0 00000  TIX   TEST IF CHARACTERS DESIRED.
00174 0020 00 0 00211  TRA   COSEQX
00175 0765 00 0 00022  LRS   18
00176 0221 00 0 00332  UVP   RIGHT ADJUST BIN INTEGER
00177 00001 00 0 00000  TIX   TEN
00178 00000 00 0 00000  TIX   EOMMAN
00179 00000 00 0 00000  TIX   PWD
00180 00000 00 0 00000  TIX   TEN
00181 00001 00 0 00000  TIX   PWD
00182 0767 00 0 00006  ALS   6
00202 0767 00 0 00006  ORS   COMMON
00203 -0602 00 0 77777  ORS   PXD
00204 -0754 00 0 00000  PXD
***** MM100770 ***** MM100771 *****
***** MM100772 ***** MM100773 *****
***** MM100774 ***** MM100775 *****
***** MM100776 ***** MM100777 *****
***** MM100778 ***** MM100779 *****
***** MM100780 ***** MM100781 *****
***** MM100782 ***** MM100783 *****
***** MM100784 ***** MM100785 *****
***** MM100786 ***** MM100787 *****
***** MM100788 ***** MM100789 *****
***** THIS ROUTINE CONVERTS A BINARY INTEGER TO BCD. (4 DIGITS DEC-R-MQ) *****
***** MM100790 ***** MM100791 *****
***** MM100792 ***** MM100793 *****
***** MM100794 ***** MM100795 *****
***** MM100796 ***** MM100797 *****
***** MM100798 ***** MM100799 *****
***** MM100800 ***** MM100801 *****
***** MM100802 ***** MM100803 *****

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00243	+00000000000102
00244	+0000000000042
00245	+0000000000000000
00246	+0000000000000000
00247	+0000000000000000
00250	+0000000000000000
00251	+0000000000000000
00252	+0000000000000000
00253	+0000000000000000
00254	+0000000000000000
00255	+0000000000000000
00256	+0000000000000000
00257	+0000000000000000
00260	+0000000000000002
00261	+0000000000000001
00262	+0000000000000000
00263	+0000000000000000
00264	+0000000000000042
00265	-3 77777 7 000
00266	0400 00 0 000
00267	+0000000000000000
00270	+0000000000000000
00271	+0000000000000000
00272	+0000000000002100
00273	+0000000000002100
00274	+0000000000002040
00275	+0000000000002020
00276	+0000000000002010
00277	+0000000000002000
00300	+0000000000002002
00301	+0000000000002001
00302	0 00000 0 000
00303	+0000000000002102
00304	+0000000000002042
00305	+0000000000000000
00306	6060606060606060
00307	0074 00 0 00
00310	+0000000000000000

00311 +0000000001400
00312 +0000000001200

00316 +0000000001010
00317 +0000000001004
00320 +0000000001002

00324 +0000000001042
00325 0 00001 0 00000 D1 0,0,1
00326 0 00000 0 00000 10LCD PLE

00332 +0000000000012 1EN DEC 10
00333 0000 00 0 00026 A22 MTR 22
00334 +000526000000 IMAGE OCT

HM100849
HM100850
HM100854
HM100855
HM100856
HM100860
HM100861

CONTROL WORD SKELETON

11116 END SYN COMMNL

POST PROCESSOR ASSEMBLY DATA

225 IS THE FIRST LOCATION NOT USED BY THIS PROGRAM

3335 IS THE FIRST LOCATION NOT USED BY THIS PROGRAM

333 13 INC 13 INC LOCATOR NO. 333			
330	SA		
325	D1	16	
54	G2	34	
70	N	161.	167
216	TB	227	
142	X1	6	
333	A22	147	
105	ABC	115,	117
77776	END	15,	55,
		136,	160
230	TAB	107	
215	IB1	134.	216.
332	TEN	176,	201,
77730	LAST	113.	214
66	LOCN	17	
327	L(11)	74,	133
305	BCDID	51,	76
6	BINPU	0	
306	BLANK	211	

POST PROCESSOR ASSEMBLY DATA

131	BPTES	140
326	IDLCD	100, 116
334	IMAGE	25
267	SEQNO	47, 73, 132, 135
7777	COMMON	162, 166, 174, 203, 207, 335
211	C0SEQX	
242	MSK2CH	
122	WRITE1	

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